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Rethel's Lumped Constants

for

Small Irises

by

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Revisions to:

Bethe's Lumped Constants for Small Irises by Frederick B. Wood

Since preparation of these notes the following points have been clarified:

Page 5, last paragraph: Bethe rejects the $\bar{K}\phi$ and $(\gamma/\epsilon)\nabla_{\perp}\phi$ terms of equations (9) and $\bar{K} \times \nabla_{\perp}\phi$ term of (10) in obtaining (15) and (16) on the basis that the differential contributions of these terms fail to satisfy the boundary conditions on the screen. He then, without explanation, doubles the value of \bar{K}_m and γ_m . The correct justification for this step is that although some differential elements in equations (9) and (10) fail to satisfy the boundary conditions, the integrated values (i.e. over the whole plane) satisfy the boundary conditions so that these terms cannot be discarded on the boundary condition argument. However in this problem the integrated contribution of \bar{K}, γ over the whole screen (including hole) equals the contribution of \bar{K}, γ_m over the plane (zero except in hole), hence the \bar{K}, γ terms can be replaced by equivalent \bar{K}_m, γ_m terms, which doubles \bar{K}_m, γ_m in equations (15) and (16).

Page 6, last paragraph: The above revision which is a more fundamental procedure substitutes multiplying $\bar{K}_m(r')$ by two instead of dividing $\bar{F}(0)$ by two, yet giving the same final results.

Page 7, second paragraph: The reversing of the sign of one field (on left) is unnecessary provided the logic of correction to page 5 is followed.

Page 7, footnote⁺: Bourgin¹⁷ in the meantime pointed out that discontinuities in currents and charges around the edge of the hole were not accounted for. Bouwkamp³ specified this condition mathematically in the form of equation (23).

Page 33A: "Indirect Measurement" means that the point for $d=0.125"$ was for an iris on the output of a resonator instead of the input as was done with the other sizes. It is planned to make a more reliable measurement of this when the equipment is available again.

May 15, 1951.

F. B. Wood

Bethe's Lumped Constants for Small Irises

The development of the theory of diffraction for small holes and application to irises in waveguides and cavity resonators, published by H. A. Bethe in M. I. T. Radiation Laboratory Reports W-155(128)^{1A} and 43-22(194)², is here summarized in rationalized M. K. S. units instead of the original Gaussian unrationalized units. It is not safe to simply transform Bethe's formulas from Gaussian unrationalized units to rationalized M. K. S. units, because he defines magnetic current density as $\vec{K} = \frac{\vec{E} \times \vec{n}}{2\pi}$ yet there are some equations in 43-22 where the 2π has been dropped and one equation where a 4π required in the unrationalized system is omitted.

For the circular aperture the correct value of the H component of magnetic current given by Bouwkamp³ is included. This error does not, however, change the radiation field and consequently it makes no change in the lumped constant polarizabilities obtained by Bethe.

As in 43-22, the equivalent magnetic and electric polarizabilities are used to obtain the Poynting vector, change of resonant frequency of a cavity, susceptance of an iris in a waveguide, and energy emitted from a cavity through aperture into free space and into a waveguide. These results differ from Bethe's results by functions of 2 and/or 2π due to discrepancies mentioned above. The iris susceptance is compared with other reliable results. The frequency shift and Q_c (coupled Q) for coupling to TE_{10} waveguide from TM_{020} cavity resonator are compared with experimental data for which the correspondence is fair. (The experimental data is from cavity measurements which were not designed to give a direct test of Bethe's theory.)

An example of emission through an iris into free space is calculated numerically, which shows that Bethe's statement "That this power is about 25 times greater for emission into free space than for emission into a waveguide of customary dimensions" is not valid. No experimental data has been obtained to check this point.

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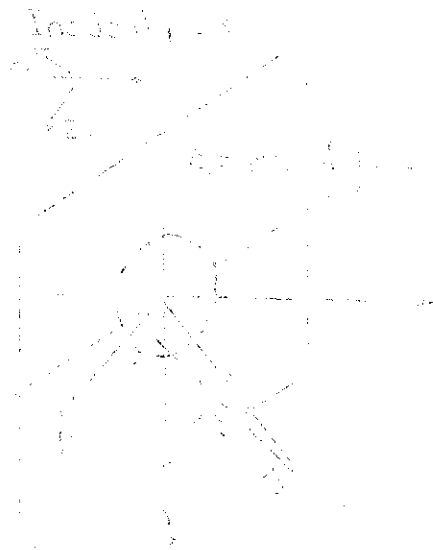
1. The Diffraction Problem.

The diffraction of electromagnetic waves by a small hole in an infinite plane conducting screen is studied first, since it is a simpler case of the problem of coupling from a resonant cavity to waveguide.

In the usual Kirchhoff method, the diffracted field is expressed in terms of the incident field in the hole, which, however, does not satisfy the boundary condition. A number of writers have set up a vector formulation of Kirchhoff's method,⁵ but this still does not satisfy the boundary condition when the integrals are taken over the aperture only.⁶ There does exist a rigorous solution by Sommerfeld for the diffraction of a semi-plane wave, with which comparisons can be made to check on the plausibility of the approximations. C. J. Bouwkamp⁷ has obtained a series solution for the diffraction problem for which the correct relation of fields is the following:

In the aperture, the fields H_{z0} and E_{z0} are given as the expansion about the aperture of the field with no existing field above the aperture. If there are incident fields on both sides, then H_{z0} and E_{z0} are the average between those on the left and the right.

4. DIFFRACTION BY WILSON'S SCREEN



Consider an observation point \$P\$ at distance \$r\$ from the hole. The wave function at \$P\$ is denoted as \$u_p(r)\$. There is a scalar potential \$V(x,y,z)\$ such that $\nabla^2 u + k^2 u = 0$. The wave function \$u\$ satisfies the Helmholtz equation. Then the wave function \$u\$ is given by the integral of the source over the volume. Then the wave function \$u\$ is given by the integral of the source over the volume.

$$u_p(r) = \frac{1}{4\pi r} \int_{\Sigma} \left[\frac{\partial u_0}{\partial z'} - u_0 \frac{\partial \phi(r')}{\partial z'} \right] \phi(r') d\Omega$$

Consider the case where the hole is small. The wave function \$u\$ is given by the integral of the source over the volume. The wave function \$u\$ is given by the integral of the source over the volume. The wave function \$u\$ is given by the integral of the source over the volume.

$$u_p(r) \approx \frac{1}{4\pi r} \left[\frac{\partial u_0}{\partial z'} \phi(r) + u_0 \frac{\partial \phi(r)}{\partial z'} \right]$$

for small hole and large \$r\$.

There are two alternative assumptions:

(a) \$u_0\$ inside = \$u_0\$ outside, then \$u_0 \neq 0\$, \$\frac{\partial u_0}{\partial z'} = 0\$ in the hole, \$\frac{\partial \phi(r)}{\partial z'} = 0\$ for \$r \gg r_0\$ on screen.

(b) \$u_0\$ inside = \$u_0\$ outside + \$u_1\$, then \$u_0 = 0\$, \$\frac{\partial u_0}{\partial z'} = 2 \frac{\partial u_1}{\partial z'}\$ in the hole, \$\frac{\partial \phi(r)}{\partial z'} = 0\$ for \$r \gg r_0\$ on screen.

So on screen at large \$r\$:

$$(a) \mu_p(r) = -\frac{A}{4\pi} \frac{\partial \mu_z}{\partial z'} \phi(r) \neq 0 \quad (b) \mu_p(r) = -\frac{A}{2\pi} \frac{\partial \mu_z}{\partial z'} \phi(r) \neq 0$$

Since $\mu = \bar{E}_z$ a component of $\bar{E} \times \bar{n}$, the boundary condition $\bar{E} \times \bar{n} = 0$ is violated.

Next we consider the vector equivalent of Poincaré's Theory by the direct integration of Maxwell's equation using the vector analogue of Green's Theorem as given by Stratton⁹ or by Silver¹⁰.

Maxwell's equations and equations of continuity for $\Omega \in \mathbb{R}^3(\omega T - kr)$

$$\begin{aligned} (a) \quad \nabla \times \bar{E} + j\omega\mu\bar{H} &= -\bar{J}_m & (b) \quad \nabla \cdot \bar{H} - j\omega\epsilon\bar{E} &= \bar{J} \\ (c) \quad \nabla \cdot \bar{H} &= \frac{j\omega\epsilon}{\mu} & (d) \quad \nabla \cdot \bar{E} &= \rho/\epsilon \\ (e) \quad \nabla \cdot \bar{J}_m + j\omega\epsilon_m &= 0 & (f) \quad \nabla \cdot \bar{J} + j\omega\rho &= 0 \end{aligned}$$

Using equations (103, 102, 111) of Silver we have at point r :

$$(a) \quad \bar{E}(r) = \begin{cases} -\frac{1}{4\pi\epsilon} \int_{\Omega} (\text{grad}' \phi + \bar{J}_m \times \nabla' \phi - \bar{J}_e \nabla' \phi) d\Omega' \\ + \frac{1}{4\pi\epsilon} \int_{\Sigma} [-\cos\mu(\bar{n} \cdot \bar{J} + j\omega\epsilon' \bar{n} \cdot \bar{E}) - \sin\mu(\bar{n} \cdot \bar{E})] \nabla' \phi d\Omega' \end{cases}$$

$$(b) \quad \bar{H}(r) = \begin{cases} -\frac{1}{4\pi\mu} \int_{\Omega} (\text{grad}' \psi + \bar{J}_e \times \nabla' \psi - \bar{J}_m \nabla' \psi) d\Omega' \\ + \frac{1}{4\pi\mu} \int_{\Sigma} [\sin\mu(\bar{n} \times \bar{J}) + (\bar{n} \cdot \bar{H}) \nabla' \psi - \cos\mu(\bar{n} \cdot \bar{H})] \nabla' \psi d\Omega' \end{cases}$$

The electric and magnetic surface currents are defined as follows:

$$(c) \quad \begin{cases} \bar{K} = \bar{n} \times \bar{H} & \eta_m = \frac{1}{\mu} \nabla' \cdot \bar{E} \\ \bar{K}_m = \bar{E} \times \bar{n} & \eta_e = \frac{1}{\epsilon} \nabla' \cdot \bar{H} \end{cases}$$

The electric and magnetic surface currents are defined as follows:

$$\bar{K} = \frac{\bar{n} \times \bar{H}}{\mu} \quad \bar{K}_m = \frac{\bar{E} \times \bar{n}}{\epsilon} \quad \eta_m = \frac{1}{\mu} \nabla' \cdot \bar{E} \quad \eta_e = \frac{1}{\epsilon} \nabla' \cdot \bar{H}$$

Since in this problem, all sources are in the plane of the screen, (r, θ) reduce to $(\rho, \phi) = -\rho \hat{\phi}$

$$E(r) = \frac{1}{4\pi\epsilon_0} \int_S \frac{1}{r^2} \hat{r} \rho(\rho, \phi) d\tau = \frac{1}{4\pi\epsilon_0} \int_S \frac{1}{r^2} \hat{r} \rho(\rho, \phi) d\tau$$

$$H(r) = \frac{1}{4\pi\epsilon_0} \int_S \frac{1}{r^2} \hat{r} \times \nabla \rho(\rho, \phi) d\tau = \frac{1}{4\pi\epsilon_0} \int_S \frac{1}{r^2} \hat{r} \times \nabla \rho(\rho, \phi) d\tau$$

Equations (1) & (2) are vector integrals over the complete boundary of the region. In the "vector equation" we must take into account that in a region V there are no charges, so that $\nabla \cdot E = 0$ and $\nabla \times H = 0$. In the region V , the vector equation is satisfied by E and H if and only if $\nabla \cdot E = 0$ and $\nabla \times H = 0$. The boundary conditions are that E and H must be continuous across the boundary. The boundary conditions are that E and H must be continuous across the boundary. The boundary conditions are that E and H must be continuous across the boundary.



3. Mathematical Formulation and Boundary Conditions.

Let \vec{H}_0 and \vec{E}_0 be the standing wave field on the left hand side of the screen if there is no hole. The boundary condition at $z=0$ is that

(11a) $\vec{n} \cdot \vec{E}_0 = 0$

(11b) - which make $\vec{n} \cdot \vec{H}_0$

$H_{0\text{normal}}$ and $E_{0\text{normal}}$ are in phase for $\vec{n} \cdot \vec{E}_0 = 0$. Similarly the diffracted field on the left is \vec{H}_1 and \vec{E}_1 respectively \vec{H}_2, \vec{E}_2 on the total field with a hole in screen.

(12)
$$\left. \begin{aligned} \vec{H} &= \vec{H}_0 + \vec{H}_1 \\ \vec{E} &= \vec{E}_0 + \vec{E}_1 \end{aligned} \right\} z < 0 \quad \left. \begin{aligned} \vec{H} &= \vec{H}_2 \\ \vec{E} &= \vec{E}_2 \end{aligned} \right\} z > 0$$

Applying (11) or (12) to the field on the left side of the screen gives the boundary conditions:

(13) $\vec{n} \cdot \vec{E}_1 = 0, \vec{n} \cdot \vec{E}_2 = 0, \vec{n} \cdot \vec{H}_1 = 0, \vec{n} \cdot \vec{H}_2 = 0$



Applying (13) to the field on the left side of the screen gives the boundary conditions:

$$E_{1z} = 0, E_{2z} = 0, H_{1z} = 0, H_{2z} = 0$$

Applying (13) to the field on the right side of the screen gives the boundary conditions:

(14) $\vec{n} \cdot \vec{E}_1 = 0, \vec{n} \cdot \vec{E}_2 = 0, \vec{n} \cdot \vec{H}_1 = 0, \vec{n} \cdot \vec{H}_2 = 0$

(15) $\vec{n} \cdot \vec{E}_1 = 0, \vec{n} \cdot \vec{E}_2 = 0, \vec{n} \cdot \vec{H}_1 = 0, \vec{n} \cdot \vec{H}_2 = 0$

Applying (14) to the field on the right side of the screen gives the boundary conditions:

(16) $\vec{n} \cdot \vec{E}_1 = 0, \vec{n} \cdot \vec{E}_2 = 0, \vec{n} \cdot \vec{H}_1 = 0, \vec{n} \cdot \vec{H}_2 = 0$

Applying (15) to the field on the right side of the screen gives the boundary conditions:

Applying (16) to the field on the right side of the screen gives the boundary conditions:

The problem now is to calculate \bar{E}_2, \bar{H}_2 subject to b.c. (11a) on screen and (11a, 11b) in the hole. Bethe states: "These conditions are valid irrespective of size and shape of hole."² This statement of Bethe's has been reviewed by Silver¹³ and these conditions (11) are found to correspond to the unique solution of the problem. Since $\frac{1}{2} H_{0tan} = H_{ican}$ and $\frac{1}{2} E_{0n} = E_{im}$ Eq. (11) is equivalent to this statement of Smythe: "When any form of electromagnetic wave strikes a thin plane perfectly conducting sheet of any shape, the normal electric and tangential magnetic fields of the original wave are unperturbed in the apertures."

Instead of assuming \bar{E}, \bar{H} in hole equal to the incident wave as in the Woff method, we shall set up some integral equations to be solved for $\bar{K}, \eta, \bar{K}_m, \eta_m$ in the hole. From (11a)(9)(10) we see that \bar{K}, η generate $\bar{E}(r), \bar{H}(r)$ which violate b.c. on screen. From (11b)(11a)(11b) $\bar{K} = \frac{1}{2} \bar{n} \times \bar{H}_0 e, \eta = \frac{\epsilon}{2} \bar{n} \cdot \bar{E}_{0n}$ which means \bar{K} and η are already known. Similarly we see that \bar{K}_m, η_m generate $\bar{E}(r), \bar{H}(r)$ which satisfy b.c. on screen and still are unknown to be determined (Only continuity is required by (13e, f)).

Using only the terms which (1) are not yet fixed in the hole and (2) satisfy b.c. on screen, we obtain eqs. \bar{K}_m and η_m . (9)(10) reduce to

$$(15) \quad \bar{E}(r) = \frac{1}{4\pi} \int_S \bar{K}_m \times \nabla_f \phi \, dS$$

$$(16) \quad \bar{H}(r) = -\frac{1}{4\pi} \int_S \left[\omega \epsilon \bar{K}_m \phi + \frac{\eta_m}{N} \nabla_f \phi \right] dS$$

S is the surface around hole in plane

¹³ There may be some confusion in the literature with respect to reference (13) and (14) which I have not yet checked.

has a problem for it. The boundary conditions are given for \vec{E} and \vec{H} which satisfy b. c. in hole (14). Putting \vec{E} and \vec{H} in terms of vector and scalar potentials as is done by Schenkoff¹⁶

$$\begin{aligned}
 (1) \quad (a) \quad \vec{E} &= (-\text{grad } \bar{A} - \dot{\nabla} V) - (\nabla \times \vec{F}) \\
 (b) \quad \vec{H} &= (\nabla \times \vec{A}) + \nabla U + j\omega \epsilon \vec{F} \\
 (c) \quad \bar{A} &= \int_V \frac{\bar{J} e^{-jkR}}{4\pi R} dV & (d) \quad V &= \int_V \frac{q_v e^{-jkR}}{4\pi \epsilon R} dV \\
 (e) \quad \vec{F} &= \int_V \frac{\vec{M} e^{-jkR}}{4\pi R} dV & (f) \quad U &= \int_V \frac{m_v e^{-jkR}}{4\pi \mu R} dV
 \end{aligned}$$

The exclusion of terms already fixed in hole and not satisfying b. c. on screen as in (15)(16) gives from (1): $\vec{M} \cdot \vec{S} = \vec{K}_m$, $dS = dV$; $m_v = \eta_m$

$$(18) \quad \vec{E}(r) = -\nabla \times \vec{F}$$

$$(19) \quad \vec{H}(r) = -\nabla U - j\omega \epsilon \vec{F}$$

$$(20) \quad \vec{F}(r) = \int_S \frac{\vec{K}_m(r') e^{-jk|r-r'|}}{4\pi|r-r'|} dS(r')$$

$$(21) \quad U(r) = \int_S \frac{\eta_m(r') e^{-jk|r-r'|}}{4\pi\mu|r-r'|} dS(r')$$

Equations (20)(21) are the integral equations to be solved for \vec{K}_m, η_m where $\vec{F}(r)$ and $U(r)$ are fixed by b.c. (14). A rigorous interpretation of (20) and (21) indicates that the integral is to be taken over the two boundary surfaces separated by the infinitesimal gap S . By b.c. (13e)(13) and opposite direction of normals on left and right: $\vec{K}_m(0^-) = -\vec{K}_m(0^+)$; $\eta_m(0^-) = -\eta_m(0^+)$. This makes $\vec{F}(0) = 0, U(0) = 0$ from (20)(21), yet by (14) we know $V(0)$ and $U(0)$ are generally non-zero. This difficulty is resolved by taking half of $\vec{F}(0)$ and $U(0)$ are integrating over the right surface only (i.e. solving for the diffracted wave to the right):

$$(20a) \quad \frac{1}{2} \vec{F}(0) = \int_S \frac{\vec{K}_m(r') e^{-jk|r-r'|}}{4\pi|r-r'|} dS(r')$$

$$(2a) \quad \frac{1}{2} U(r,0) = \int_{S_0} \frac{\gamma_m \bar{e}^{-jk|r-r'|}}{4\pi|r-r'|} dS(r')$$

This can be put in the form:

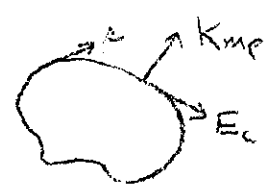
$$\bar{F}(r,0) = \int_{S_0} \frac{\bar{E} \times \bar{n}}{2\pi} \frac{e^{-jk|r-r'|}}{|r-r'|} dS(r')$$

Bethe (1) uses this form (not used in this paper) and (2) uses $\bar{K}_m = \frac{\bar{E} \times \bar{n}}{2\pi}$ and $\gamma_m = \frac{\bar{H} \cdot \bar{n}}{2\pi}$ in gaussian units. In gaussian units $\text{div } \bar{H} = 4\pi \rho = 4\pi \frac{\gamma_m}{\delta}$ so the above definition of γ_m can be derived by reversing the sign of the fields on the left which gives $\text{div } \bar{H} = \frac{2\bar{H} \cdot \bar{n}}{\delta}$ so $\gamma_m = \frac{\bar{H} \cdot \bar{n}}{2\pi}$. This means that γ_m in Bethe's definition includes the "magnetic charges" associated with both the diffracted waves to the left and to the right. This means that Bethe's development and this paper give consistent values of $\bar{E} \times \bar{n}$ and $\bar{H} \cdot \bar{n}$, yet Bethe's equations give twice the values of \bar{K}_m and γ_m defined in this paper.

$\bar{n} \cdot \text{into (6a) gives: } \nabla \cdot (\bar{E} \times \bar{n}) = -j\omega\mu(\bar{m} \cdot \bar{n})$ or

$$(22) \quad \nabla \cdot \bar{K}_m = \frac{\partial K_{mx}}{\partial x} + \frac{\partial K_{my}}{\partial y} \quad \nabla \cdot \bar{K}_m = -j\omega\gamma_m$$

For an infinite plane wave at an infinite plane screen \bar{H}_0 is constant over the hole. In actual practice and particularly for waveguides the standing wave \bar{H}_0, \bar{E}_0 will vary across the aperture. When $ka \ll 1$, where a is the farthest point of the aperture edge from center of gravity, taking \bar{H}_0 as constant is still a good approximation for simplifying $U(r,0)$ for use in (21a) to solve for γ_m . Caution must be observed to avoid neglecting the curl \bar{H} so that no important components of \bar{E} are lost.



On the contour of the hole the b.c. $\bar{E} \times \bar{n} = 0$ on the screen requires E_{tan} vanish on the contour

$$(23)* \quad \bar{E}_c = \bar{E} \cdot \bar{a} = 0 \text{ on contour}$$

*This condition was not included in Bethe's original paper^{1a,1b} but was published by Bethe in an M.I.T. R.L. report which remained classified for some time. Bourgin¹⁷ in the meantime (published this condition) said some condition like this was necessary.

The magnetic current perpendicular to contour must likewise vanish.

$$(24) \quad \bar{K}_{mp} = \bar{E}_L \times \bar{n} = \bar{E} \cdot (\bar{a} \times \bar{n}) = -\bar{n} \times (\bar{E} - \bar{a}) = 0, \quad K_{mp} = 0 \text{ on } C$$

From (23) we have: $\oint \bar{E} \cdot d\bar{a} = 0 \quad \dots (25a)$

By Stoke's Law: $\oint \bar{E} \cdot d\bar{a} = \int_A (\nabla \times \bar{E}) \cdot \bar{n} \, da$

From (6)(2)(25a) $0 = \oint \bar{E} \cdot d\bar{a} = -j\omega\mu \int_A \bar{H} \cdot \bar{n} \, da = -j\omega \int_A \eta \, da$

$$(25b) \quad \int_A \eta \, da = 0$$

The total "magnetic charge" or the window is zero.

4. Separation into H and E Components.

Examination of (22) indicates division of fields into two components is possible. $\bar{K}_m = \bar{K}_{mH} + \bar{K}_{mE}$

$$\text{div } \bar{K}_H = -j\omega \eta_m \neq 0$$

$$\text{div } \bar{K}_E = 0$$

$$\text{curl } \bar{K}_H \sim k_a \cos \theta \text{ curl } \bar{K}_E \neq 0$$

$$\text{curl } \bar{K}_E \neq 0$$

$$* \theta < \theta \leq 90^\circ, B \sim 20^\circ$$

θ is angle of incidence (to normal) of path of incident wave: $k_a \ll 1$

Using "N" to mean "order of magnitude of" where $k_a \ll 1$:

$$(23a) \quad \frac{1}{2} \bar{F} = \int_{S_1} \frac{\bar{K}_m(r') dS(r')}{4\pi |r-r'|} \sim \sqrt{k_a} a \quad \dots (26a)$$

$$(24a) \quad \frac{1}{2} U = \int_{S_2} \frac{\eta_m(r') dS(r')}{4\pi \mu |r-r'|} \sim \frac{\eta_m a}{\mu} \quad \dots (26b)$$

Considering the two components:

(1) H component

$$\nabla \cdot \bar{K}_m \sim k_a \sim \omega \eta_m \quad (27a)$$

$$K_m \sim \omega a \eta_m \quad (28a)$$

$$K_m \sim k_a \sqrt{\frac{\mu}{\epsilon}} (\bar{H} \cdot \bar{n})$$

$$E_{tm}(r') \ll \sqrt{\frac{\mu}{\epsilon}} H_{tm}(r')$$

Electric dipoles neglected ($B < \theta \leq 90^\circ$)

$$\bar{H}(r) \sim [1/(k_a^2)] \frac{\eta_m}{\mu}$$

$$\boxed{\bar{H}(r) = -\nabla U} \quad (29a)$$

$$E(r) \ll \sqrt{\frac{\mu}{\epsilon}} H(r)$$

Normal $\bar{H}(r)$ predominates, which is generated by incident tangential \bar{H}_m

$$\eta_m \sim \mu H_b \quad (30a)$$

(2) E component

$$\nabla \cdot \bar{K}_E = 0 \quad (27b)$$

$$\eta_m = 0 \quad (28b)$$

$$(\bar{H} \cdot \bar{n}) = 0$$

$$H_n(r') = 0 \quad E_{tn}(r') \text{ is present}$$

Magnetic dipoles not present

$$\nabla U = -j\omega \epsilon \bar{F}$$

$$U = 0; \quad H(r) \sim k_a \sqrt{\frac{\mu}{\epsilon}} K_m$$

$$\boxed{E(r) = -\nabla \times \bar{F}} \quad (29b)$$

$$E(r) = -\nabla \cdot \bar{F} \sim \frac{\mu}{\epsilon} \sim K_m$$

$$\sqrt{\frac{\mu}{\epsilon}} H(r) \ll E(r)$$

Tangential $\bar{E}(r)$ predominates, which is generated by incident normal \bar{E}_m .

$$K_m \sim E_b \quad (30b)$$

5. Solution for the H component.

We neglect terms of order ka since in this approximation $ka \ll 1$.

For uniform incident field by b.c. (14a) and (29a) we have at $z = 0$:

$$(31) \quad \bar{H} = \frac{1}{2} \bar{H}_{0y} = -\nabla U = -\bar{a}_y \frac{\partial U}{\partial y} \quad U = -\int \frac{H_{0y}}{2} dy = -\frac{1}{2} H_{0y} y = -\frac{1}{2} \bar{H}_0 \cdot \bar{r}$$

(31) in (26b) gives integral equation for η_m :

$$(32) \quad -\frac{1}{4} \bar{H}_0 \cdot \bar{r} = \int_{S_0} \frac{\eta_m(r')}{4\pi\mu |r-r'|} dS(r')$$

The magnetic moment is:

$$(33) \quad \bar{X} = \int_{S_0} \eta_m(r') \bar{r}' dS(r')$$

$$\bar{r}' = \bar{a}_x x' + \bar{a}_y y'$$

Using $\bar{r}' = \bar{a}_x x' + \bar{a}_y y'$ and (22) in (33).

$$\bar{X} = \bar{a}_x X_x + \bar{a}_y X_y = \bar{a}_x \int_{S_0} \eta_m(r') x' dS + \bar{a}_y \int_{S_0} \eta_m(r') y' dS$$

$$-j\omega X_x = \int_{S_0} x (\nabla \cdot \bar{K}_m) dS \quad -j\omega X_y = \int_{S_0} y (\nabla \cdot \bar{K}_m) dS$$

$$-j\omega X_x = \int x (\nabla \cdot \bar{K}_m) dS = \int \nabla \cdot (x \bar{K}_m) dS - \int \bar{K}_m (\nabla x) dS \quad (35)$$

$$\stackrel{!}{=} \text{term by Gauss law and (24): } \int_{S_0} \nabla \cdot (x \bar{K}_m) dS = \int (x \bar{K}_m)_p dA = 0$$

$$\therefore \boxed{j\omega \bar{X} = \int \bar{K}_m dS} \quad (36) \quad \text{or} \quad \boxed{j\omega \bar{X} = -\bar{n} \times \int \bar{E} dS} \quad (36a)$$

By (36) \bar{X} is a magnetic dipole moment in the plane of the screen.

It is known, if E_{tan} over aperture is known. (As will be shown in the next section, the electric dipole and hence the complete solution determined by E_{tan} over the aperture.)

Examination of (32)(33) shows that η_m and \bar{X} are linear functions of H_{0x} and H_{0y} ; so we write \bar{X} in terms of \bar{M} , the components of a magnetic polarizability tensor.

$$\begin{aligned}
 X_x &= \vec{M}_{xx} H_{0x} + \vec{M}_{xy} H_{0y} \\
 (3) \quad X_y &= \vec{M}_{yx} H_{0x} + \vec{M}_{yy} H_{0y}
 \end{aligned}$$

The originally incorrect sign of M was corrected by Bethe¹⁸. The sign can be found from the following development related to Stratton's discussion of Poynting's Theorem¹⁹. The stored energy is:

$$(38a) \quad W = \frac{1}{2} \int_V [\vec{E} \cdot \vec{D} + \vec{H} \cdot \vec{B}] dV \quad \text{/inst}$$

In the equations marked "/inst" the field vector \vec{E} , \vec{D} , \vec{H} , \vec{B} are the instantaneous real values. In general in this paper, the field vectors indicate the peak values (or the field vector with the time factor $e^{j\omega t}$ omitted). Eq (38a) is also valid where \vec{E} , \vec{D} , \vec{H} , \vec{B} are average values.

Substituting (18)(17)(6a)(6c) into (38a)

$$(39a) \quad W_{av} = \frac{1}{2} \int_V \left\{ -\epsilon \nabla \cdot (\vec{F} \times \vec{E}) + j\omega \rho_m \vec{E} \cdot \vec{F} + \epsilon \vec{F} \cdot \nabla \times \vec{E} - \mu \nabla \cdot (\vec{F} \times \vec{H}) - j\omega \rho_m \vec{H} \cdot \vec{F} + \mu \vec{F} \cdot \nabla \times \vec{H} \right\} dV \quad \text{(19)}$$

$$(39b) \quad \frac{1}{2} W_{av} = \frac{1}{2} \int_V \left(\epsilon \vec{J}_m \cdot \vec{F} + U \rho_m \right) dV + \frac{1}{4} \int_{S_2} (\vec{F} \times \vec{E} \cdot \vec{n} + \vec{F} \times \vec{H} \cdot \vec{n}) dS \quad \text{(20)}$$

The second 1/2 comes from division at $z = 0$ as in (20a)(21a). The volume is bounded by a hemisphere on the right and the conducting surface of the screen plus a surface through aperture. Since the waves are propagated by a finite velocity, we may take the radius of the hemisphere sufficiently large so that the diffracted wave has not reached the surface yet, then the second integral is zero over the hemisphere. The surface integral over the screen is zero since $\vec{F} \times \vec{E} \cdot \vec{n} = 0$ and $\vec{F} \times \vec{H} \cdot \vec{n} = 0$ or so on. This leaves

$$\begin{aligned}
 (39c) \quad \frac{1}{2} W_{av} &= \frac{1}{2} \int_V (\epsilon \vec{J}_m \cdot \vec{F} + U \rho_m) dV \\
 W_{av} &= \int_V (\epsilon \vec{J}_m \cdot \vec{F} + U \rho_m) dV
 \end{aligned}$$

change from instantaneous $\hat{I}_m, \hat{F}, \hat{U}, \hat{z}_m$ to peak values.

$$(40) \quad \frac{1}{2} W_{\omega} = \frac{1}{8} \int_{S} [U \eta_m + \epsilon \bar{F} \cdot \bar{K}_m] dS$$

For H component by (29a) second term is of order $(ka)^2$, $ka \ll 1$ so by (21a)

$$(40a) \quad W_{\omega} \approx \frac{1}{8} \int_{S} U \eta_m dS = \frac{1}{8\pi\mu} \iint \frac{\eta_m(r) \eta_m(r')}{|r-r'|} dS(r) dS(r') > 0$$

(40a) is positive since it is a self potential. Using (40a)(32)(33):

$$W_{\omega} = -\frac{1}{8\pi\epsilon} \int \bar{H}_0 \cdot \bar{r} \eta_m dS = -\frac{\bar{H}_0}{8\pi\epsilon} \cdot \int \bar{r} \eta_m dS = -\frac{\bar{H}_0 \cdot \bar{\chi}}{8\pi\epsilon} > 0$$

So \bar{H} and $\bar{\chi}$ have opposite signs

$$(41) \quad \underline{W_{\omega} = -\frac{1}{8\pi\epsilon} \bar{H}_0 \cdot \bar{\chi} > 0}$$

Let $M_{ij} = -\bar{M}_{ij}$ in (37) then: $M_{ij} > 0$

$$(41b) \quad \begin{cases} \chi_x = -M_{xx} H_{0x} - M_{xy} H_{0y} \\ \chi_y = -M_{yx} H_{0x} - M_{yy} H_{0y} \end{cases}$$

Bethe points out that the energy relation (41) is analogous to that of the ordinary theory of magnetism: "Therefore, just as we can conclude that the tensor of magnetic permeability is symmetrical, so we believe that in our case we can conclude that the M -tensor is symmetrical." #20

$$(42) \quad M_{yx} = M_{xy}$$

We need only assume that $\bar{\chi}$ is the derivative with respect to \bar{H}_0 of:

$$(42a) \quad \delta W = \frac{1}{2} M_{xx} H_{0x}^2 + \frac{1}{2} (M_{xy} + M_{yx}) H_{0x} H_{0y} + \frac{1}{2} M_{yy} H_{0y}^2$$

If we accept (42) the tensor M can be transformed to principal axes. For non-symmetrical apertures the directions of the principal axes must be determined from the integral equation.

Let \bar{l} and \bar{m} be unit vectors in the directions of the two principal axes, and H_{0l} , H_{0m} be respective components of H_0 . Then in terms of principal axes, the magnetic moment is:

$$(13) \quad \bar{\chi}_{(\text{dipole})} = -M_1 H_{0l} \bar{l} - M_2 H_{0m} \bar{m}$$

M_1, M_2 are the principal magnetic polarizabilities in units of permeability times volume ($M \sim \mu a^3$ henry-meter³)

An alternate form from (36b) is:

$$(14) \quad \bar{\pi} \times \int \bar{E} dS = +j\omega (M_1 H_{0l} \bar{l} + M_2 H_{0m} \bar{m})$$

6. Solution for E component.

For the electric component we have from (22)(2 b):

$$(45) \quad \eta_m = \frac{+j}{\omega} \nabla \cdot \bar{K}_m = \frac{j}{\omega} \nabla \cdot (\nabla \times \bar{E}) = 0$$

This means that lines of magnetic current must be closed or that \bar{K}_m can be derived from a potential function:

$$(46) \quad \bar{E}_t = -\nabla \phi$$

(45) and (46) are true irrespective of size of hole. By b.c. (23):

$\phi =$ constant on the contour of any tube. The constant may be taken as zero without changing E_z from (1.6): $\phi = 0$ on contour (46a)

$$(47)(47a) \quad -\nabla \times \bar{F} = \frac{1}{2} \bar{E}_{0z} \quad -(\nabla \times \bar{F}) \times \bar{r} = \frac{1}{2} \bar{E}_{0z} \times \bar{r}$$

$$(\nabla \times \bar{F}) \times \bar{r} = \bar{F} (\nabla \cdot \bar{r}) - \bar{r} (\nabla \cdot \bar{F}) \quad \nabla \cdot \bar{F} = 0, \nabla \cdot \bar{r} = 2 \text{ (cylindrical)}$$

$$-2\bar{F} = \frac{1}{2} \bar{E}_{0z} \times \bar{r} \quad \bar{F} = -\frac{1}{4} \bar{E}_{0z} \times \bar{r} \quad (46b)$$

Now (46b) and (23a)(23b) give the \bar{K}_m term equation to be solved $-\bar{K}_m$

$$-\frac{1}{2} \bar{E}_{0z} \times \bar{r} = \int_{\Omega} \frac{\bar{K}_m(\rho)}{4\pi} dS(\rho) \quad (46c)$$

Given $\bar{K}_m = \bar{E}_{0z} \times \bar{r}$ on the circular boundary the region we may choose is the cylinder. The cylindrical expansion of the vector \bar{r} to see what \bar{E} consists of radial and tangential components. This position is similar to that of electrostatics where \bar{r} is used in place of \bar{r} since the current is in the z direction. The current is in the z direction. The current is in the z direction, so \bar{K}_m is in the z direction. In eq. (4.0)

$$(47a) \quad \nabla^2 \bar{F} = -\bar{K}_m \in \sum_{j=1}^N \bar{F}_j = -M_j = -\frac{X_j}{\mu}$$

The dipole magnetization \bar{X} is used here and everywhere in this paper instead of loop magnetization \bar{M} to make the inhomogeneous wave equations of identical form for both magnetic and electric currents.

$$(4/b) \quad \bar{X}_0 = \bar{X} = -\frac{j \bar{J}_m}{\omega} = -\frac{j \bar{J}_m}{\omega \epsilon_0}$$

corresponding to iteration, eq. (34)

$$(4/c) \quad \bar{\Pi}^* = \frac{e^{-jkR}}{4\pi R} \int \bar{X}_0(\bar{r}') e^{+jk\bar{r}' \cdot \bar{r}} d\bar{v}'$$

The total field is $\bar{\Pi}^* = \sum_{n=0}^{\infty} \bar{\Pi}^{*(n)}$ where $\bar{\Pi}^{*(0)}$ is magnetic vector potential represented by a current and $\bar{\Pi}^{*(1)}$ is electric quadrupole, (with electric dipole contribution)

Then substituting \bar{X}_0 for \bar{M} in eq. (34) using appropriate signs of eq. (34) p. 232, eq. (34) is: $\bar{X}_0 = -\frac{j \bar{J}_m}{\omega}$

$$(4/d) \quad \bar{\Pi}^{*(1)} = \frac{1}{4\pi R} \bar{X}^{(1)} = \frac{j \bar{J}_m \cdot \bar{r}}{\omega R} \quad \bar{X}^{(1)} = \int_{ns} \bar{X}_0 dS \quad (47e)$$

$$\text{From (47d) } \bar{X}_0 = \bar{J}_m \cdot \bar{r} = \frac{-j \bar{J}_m}{\omega} = -\frac{j}{\omega} (\bar{a}_x J_x - \bar{a}_y J_y) \quad (47f)$$

(47d) is by (360)

$$\bar{X}^{(1)} = \frac{1}{4\pi R} \int \bar{E}_t dS = -\frac{1}{4\pi R} \int \nabla \phi dS = -\frac{1}{4\pi R} \int \bar{a}_y dS$$

$$\int \bar{E}_t dS = -\int \nabla \phi \cdot \bar{n} \times d\bar{a} \quad \bar{X}^{(1)} = 0 \quad (47g)$$

This vector is the electric dipole moment of the charge distribution.

The electric dipole moment of the charge distribution is

$$\bar{P} = \frac{+jk}{4\pi\omega} \left(\frac{1}{R} - \frac{j}{kR^2} \right) e^{+j(\omega t - kR)} \int \bar{r}' \rho(\bar{r}', t) d\bar{v}' \quad (48)$$

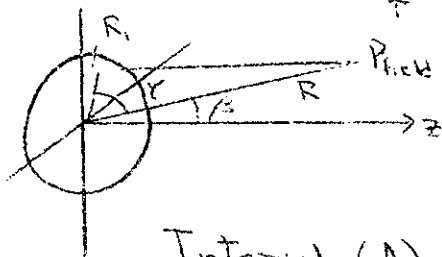
Exp. (48) in eq. (47d)

$$\bar{X}^{(1)} = \frac{1}{2R} \left[\bar{r}_1 \times \bar{X}_0 \right] \times \bar{R} + \bar{X}_0 (\bar{r}_1 \cdot \bar{R}) + \bar{R} (\bar{r}_1 \cdot \bar{X}_0) \quad (48a)$$

Changing to surface integral, the integral part of (48a) becomes.

$$\int_{ns} \vec{X}_0 R_1 \cos \gamma dS = \int_{ns} \frac{(\vec{R}_1 \times \vec{X}_0) \times \vec{R}}{2R} dS + \int_{ns} \frac{\vec{X}_0 (\vec{R}_1 \cdot \vec{R})}{2R} dS \quad (49c)$$

$$+ \int_{ns} \frac{R_1 (\vec{R}_1 \cdot \vec{X}_0)}{2R} dS \quad (c)$$



Integral (A) of (49c):

$$\int_{ns} \frac{(\vec{R}_1 \times \vec{X}_0) \times \vec{R}}{2R} dS = -\frac{j}{\omega} \int_{ns} \frac{E_x x + E_y y}{z} dx dy \vec{a}_z \times \left(\frac{\vec{R}_1}{R}\right) =$$

$$\int E_x x dS = -\int \frac{\partial \phi}{\partial x} dS = -\int \left[\frac{\partial}{\partial x} (\phi x) - \phi \right] dS$$

$$= + \int \phi dS - \int (\phi x) \cos(\vec{a}_z, \vec{R}) dz$$

by (46a) $\int E_x x dS = \int E_y y dS = \int \phi dS \quad \dots (49d)$

Integral (B) of (49c).

$$\int_{ns} \frac{\vec{X}_0 (\vec{R}_1 \cdot \vec{R})}{2R} dS = -\frac{j}{\omega} \int_{ns} (\vec{a}_x E_y - \vec{a}_y E_x) \frac{(xX_0 + yY_0)}{zR} dx dy = -\frac{j}{\omega} \left\{ \vec{a}_x \frac{Y_0}{R} - \vec{a}_y \frac{X_0}{R} \right\}$$

Integral (C) of (49c)

$$\int_{ns} \frac{R_1 (\vec{R}_1 \cdot \vec{X}_0)}{2R} dS = -\frac{j}{\omega} \int_{ns} \left(\frac{\vec{a}_x x - \vec{a}_y y}{z} \right) \left(\frac{R_1}{R} E_y - \frac{Y_0}{R} x \right) dS = \frac{j}{\omega} \left\{ \vec{a}_x \frac{Y_0}{R} - \vec{a}_y \frac{X_0}{R} \right\}$$

By (49a) (49b) integrals (B) or (C) cancel leaving (A). Putting in (49d)

(49b) back into (49c) we have:

$$(49c) \vec{\Pi}^{(1)} = \frac{j}{4\pi\epsilon_0} \frac{1}{r} \left[\vec{a}_z \int \phi dS \right] \times \nabla R \left(\frac{1}{R} - \frac{\partial}{\partial t} \right) e^{j(\omega t - \beta R)} ; \quad \vec{R} = \left(\frac{\vec{R}_1}{R} \right)$$

Comparing (49c) with Stratton, p. 496, eq. (21), $\vec{\Pi}^{(1)} \rightarrow \frac{j}{4\pi\epsilon_0} \frac{1}{r} \int \phi dS$ to see that $\vec{\Pi}^{(1)}$ is the contribution of an electric dipole of moment

$$(49d) \quad \vec{\Pi}^{(1)} = \vec{a}_z \epsilon \int \phi dS$$

Since the other integrals cancel, there is no magnetic quadrupole term from the z component. By (49b) and (49d).

$$(50) \quad \boxed{\bar{P}^{(a)} = \bar{a}_z \frac{\epsilon}{2} \int_{ns} \bar{E} \cdot \bar{r}' dS(r')} \quad \left(\bar{E}_r \text{ comes from solution of (46)} \right)$$

In §4 it was shown that the \bar{P} component is generated by the incident normal $\bar{E}(r)$. Consequently we take \bar{P} proportional to normal incident \bar{E} .

$$(51) \quad \boxed{\bar{P} = \bar{n} P(\bar{E}_0 \cdot \bar{n})}$$

P is the electric polarizability of the aperture. $P \propto \epsilon a^3$ (farad-meter³)

Alternately (50) can be obtained from \bar{K}_m directly. Examining

$$\bar{m} = \frac{\bar{X}}{\mu} = \frac{1}{2} \int_V \bar{r} \times \bar{J} dV \quad \text{in Stratton's } n^{22} \text{ and noting sign difference for (6a,b):}$$

$$(50a) \quad \bar{P}_{1/2} = \frac{1}{2} \int \bar{K}_m \times \bar{r} dS$$

$$(50b) \quad \bar{P} = \frac{\epsilon}{2} \int (\bar{E} \times \bar{n} \times \bar{r}) dS = \frac{\epsilon}{2} \int [\bar{n}(\bar{E} \cdot \bar{r}) - \bar{r}(\bar{E} \cdot \bar{n})] dS = \bar{a}_z \frac{\epsilon}{2} \int \bar{E} \cdot \bar{r}' dS$$

Note (50b) is same as (50). To determine sign of \bar{P} in (51) we use (46,47)

$$(52) \quad \frac{1}{2} \delta W_{rr} = \int_{ns} \epsilon \bar{E} \cdot \bar{K}_m dS$$

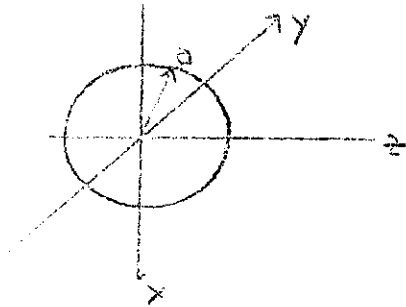
$$(53) - \text{from (46)(52)} \quad \frac{1}{2} W_{rr} = \frac{\epsilon}{4\pi} \iint \frac{\bar{K}_m(r) \cdot \bar{K}_m(r')}{|r-r'|} dS(r) dS(r') > 0$$

$$\text{From (53)(52)(46)} \quad \frac{1}{2} \delta W_{rr} = \int_{ns} (-\frac{1}{4} \bar{E}_0 \cdot \bar{r}) \cdot \bar{K}_m dS = \frac{\epsilon}{4} \bar{E}_0 \cdot \int \bar{K}_m \times \bar{r} dS$$

$$\frac{1}{2} W_{rr} = \frac{\epsilon}{32} \bar{E}_0 \cdot \left(\frac{2\bar{P}}{\epsilon} \right) = \frac{\bar{E}_0 \cdot \bar{n}}{16} P(\bar{E}_0 \cdot \bar{n}) = \frac{1}{16} P(\bar{E}_0 \cdot \bar{n})^2 > 0 \quad (54)$$

Since $(\bar{E}_0 \cdot \bar{n})^2$ is positive, P is positive. The difference in sign between \bar{P} and \bar{P}' is not due to their being magnetic and electric, but due to being parallel and perpendicular to screen.

Example of Circular Aperture.



Bethe² has obtained a solution for a circular aperture of radius a . Rowkamp³ has corrected Bethe's solution which gave incorrect H_{\tan} for H component near aperture and found Bethe's radiation field results to be correct.

Rowkamp has also obtained a series solution of which the first term corresponds to Bethe's approximation developed here.

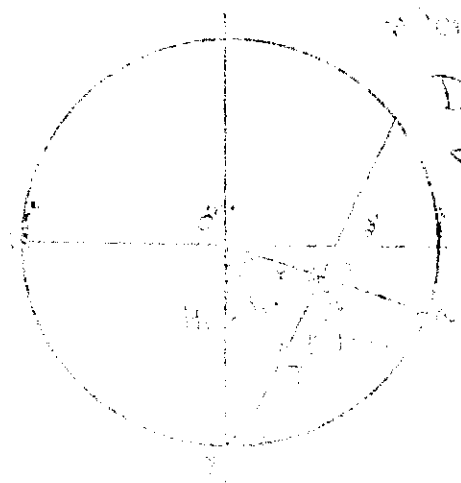
a. E Component. (Corresponds to TE mode circular iris of Stratton²⁴)

The integral equation is (32):

$$(55)(32) \quad -\frac{1}{4} \overline{H}_0 \cdot \hat{z} = \int_{S_0} \frac{\eta_m(\mathbf{r}')}{4\pi|\mathbf{r}-\mathbf{r}'|} \delta S(\mathbf{r}') d\mathbf{r}'$$

Since Rowkamp's correct solution in double spheroidal coordinates has not yet been published (to appear in second of two papers), we will outline Bethe's procedure and then give the correct solution given without formal development in Rowkamp's first paper.

Define a slab, that is constant and the field is produced by a uniform distribution of dipoles in an ellipsoid as is developed by Stratton²³. We consider the structure to be filled by an ellipsoid of semi-axes $a, b,$



where $h \rightarrow 0$ $\frac{a^2}{a^2} + \frac{z^2}{h^2} = 1$ $z \in (a^2 - r^2)^{1/2}$

Dipole surface density $\bar{X} = \alpha \bar{H}_0$ (56)

Surface charge density $\eta_m = \nabla \cdot \bar{X} = \alpha \cdot \nabla \cdot \bar{H}_0$

$\text{div} \cdot \bar{J} \bar{A}_1 = \bar{J} \cdot \nabla \bar{A}_1$ for $\bar{A} = \nabla \bar{A}$

$\eta_m = \bar{H}_0 \cdot \alpha \nabla \cdot \bar{z}$ (57)

$\eta_m = \frac{\bar{H}_0 \cdot \bar{r}'}{(a^2 - r'^2)^{1/2}}$ $\eta_m = \alpha \frac{\bar{H}_0 \cdot \bar{r}'}{(a^2 - r'^2)^{1/2}}$ (58)

$$\vec{H}_0 \cdot \vec{r}' = H_0 r + \mu \rho \cos(\alpha - \gamma) \quad (56)$$

$$(56) \text{ in } (55) \quad -\frac{1}{4} \vec{H}_0 \cdot \vec{r} = \alpha \int_0^{2\pi} \frac{d\beta}{4\pi\mu} \int_0^{\rho} \frac{H_0 r + H_0 \rho \cos(\alpha - \beta)}{(a^2 - r'^2)^{3/2}} \rho d\rho \quad (57)$$

$$\vec{r} = \rho + r \cos \beta, \quad \rho = \vec{r} - r \cos \beta, \quad d\rho = d\vec{r} \quad (\text{Combining RP, PS makes } 2\pi \rightarrow \pi)$$

$$-\frac{1}{4} \vec{H}_0 \cdot \vec{r} = \alpha \int_0^{\pi} \frac{d\beta}{4\pi\mu} \left\{ \vec{H}_0 \cdot \vec{r} \int_{-r}^{\rho} \frac{ds}{(a^2 - r'^2)^{3/2}} + H_0 \cos(\alpha - \beta) \int_{-r}^{\rho} \frac{\vec{r} ds}{(a^2 - r'^2)^{3/2}} - H_0 \cos(\alpha - \beta) \int_{-r}^{\rho} \frac{r ds}{(a^2 - r'^2)^{3/2}} \right\} \quad (58)$$

Integrals I, II are $\pi, -\pi$ by Rec. (27); III is zero by Rec. (22)

$$-\frac{1}{4} \vec{H}_0 \cdot \vec{r} = \frac{\alpha}{4\pi\mu} \int_0^{\pi} (\vec{H}_0 \cdot \vec{r} - H_0 r \cos(\alpha - \beta)) d\beta = \frac{\alpha \pi}{2\pi\mu} (\frac{1}{2} \vec{H}_0 \cdot \vec{r})$$

$$\alpha = \frac{2\mu}{\pi}$$

$$(56) \text{ in } (57) \quad \boxed{\gamma_m = -\frac{2\mu}{\pi} \frac{H_0 \cdot \vec{r}}{(a^2 - r'^2)^{3/2}}} \quad \text{(Weber's vector)} \quad (59)$$

To obtain the correct value for \vec{K}_{mH} , we have to go back to (21). Bethel had calculated \vec{K}_{mH} from (22) $\vec{K}_{mH} = \int \vec{r}' \cdot \vec{r} \gamma_m$ and thereby missed part of \vec{K}_{mH} which caused \vec{K}_{mH} to fail to set h.c. (24) $\vec{K}_{mH} = 0$ on circle $r=a$. Boukharov³ has obtained the following result as the first term in power series in (kr) in elliptic cylindrical coordinates:

$$(55) \quad \boxed{\vec{K}_{mH} = -\frac{2\mu}{\pi} \frac{H_0}{\sqrt{a^2 - x^2 - y^2}} + \frac{2\mu}{3\pi} \frac{(a^2 - x^2 - 2y^2) H_0}{\sqrt{a^2 - x^2 - y^2}}} \quad (60)$$

$$-\frac{2\mu}{\pi} \frac{H_0}{\sqrt{a^2 - x^2 - y^2}} + \frac{2\mu}{3\pi} \frac{(a^2 - x^2 - 2y^2) H_0}{\sqrt{a^2 - x^2 - y^2}} \quad (61)$$

Thus (59) agrees with (61c).

b. Electric dipole moment. The dipole moment \vec{p} is circular in the xy plane.

Boukharov did not find the dipole moment in his first paper. Since Bethel's \vec{K}_{mH} had the form of the dipole moment calculated by Boukharov, we shall use the Boukharov's result to calculate \vec{p} .

From (46c) the integral equation is:

$$(59)(46c) \quad -\frac{1}{8} \bar{E}_{\text{ext}} \cdot \bar{r} = \int_{S_1} \frac{\bar{K}_{ME}(r')}{4\pi|r-r'|} dS(r')$$

$$(59a) \quad -\frac{1}{8} E_y = \int_{S_1} \frac{K_y dS}{4\pi|r-r'|}$$

$$(55) \quad -\frac{1}{4} H_{0y} = \int_{S_1} \frac{m_m/\mu dS}{4\pi|r-r'|}$$

Comparing components with (55) : I see that they are the same equations with different symbols, so we can use (57d) which gives by comparison:

$$(60) \quad \bar{K}_{ME} = \frac{1}{\pi (a^2 - r'^2)^{3/2}} \bar{r}' \times \bar{E}_0 \quad (\text{volts})$$

c. Magnetic Polarizability.

$$(61) \quad \bar{X} = -\frac{1}{2} \int (\bar{K}_{MH} + \bar{K}_{ME}) dS \quad - \text{from (57d)(57e)}$$

The x-component of \bar{K}_{MH} and the y-z components of \bar{K}_{ME} will both integrate to zero.

It is simpler to use (33) and (57a):

$$\bar{X} = \int_{S_1} \bar{K}_{MH} \cdot \bar{r}' dS + \int_{S_1} \bar{K}_{ME} \cdot \bar{r}' dS = \bar{a}_y \int_{S_1} \bar{K}_{MH} \cdot \bar{r}' dS + \bar{a}_y \int_{S_1} \frac{E_0}{4\pi} \frac{r'^2 \cos \theta d\Omega}{(a^2 - r'^2)^{3/2}}$$

$$(62) \quad \bar{X} = -\bar{a}_y \frac{4\pi \mu H_0}{\pi} \int_{S_1} \frac{r'^2 \cos \theta d\Omega}{(a^2 - r'^2)^{3/2}} = -\bar{a}_y \frac{4\pi \mu H_0}{\pi} \int_0^{\pi/2} \int_0^{2\pi} \frac{r'^2 \cos \theta d\Omega}{(a^2 - r'^2)^{3/2}} = -\frac{4}{3} a^3 \mu H_0$$

$$(63) \quad M_y = -\frac{\bar{X}}{H_0} = \boxed{\frac{4}{3} a^3 \mu = M_{yy}}$$

d. Magnetic Polarizability.

$$(57d)(57e) \quad \bar{P} = \int_{S_1} \bar{E} \cdot \bar{r}' dS = \int_{S_1} (\bar{n} \times \bar{K}_{ME}) \cdot \bar{r}' dS = \int_{S_1} \frac{E_0}{4\pi} \frac{(\bar{n} \times \bar{r}') \cdot \bar{r}'}{(a^2 - r'^2)^{3/2}} dS$$

$$(57d)(57e) \quad \bar{P} = \frac{E_0}{4\pi} \int_{S_1} \frac{(\bar{n} \times \bar{r}') \cdot \bar{r}'}{(a^2 - r'^2)^{3/2}} dS = \frac{E_0}{4\pi} \int_{S_1} \frac{r'^2 \cos \theta d\Omega}{(a^2 - r'^2)^{3/2}} = \frac{E_0}{4\pi} \frac{4}{3} a^3$$

$$\bar{P} = +\frac{2a^3}{3} \epsilon E_0 \quad (64) \quad \bar{P} = \frac{\bar{P}}{E_0} = \boxed{+\frac{2a^3}{3} \epsilon = P}$$

8. Summary of Results for Various Shapes.

a. Circular Aperture. Radius a

Bethe's Gaussian System

$$\bar{K} = \frac{\bar{E} \times \bar{n}}{2\pi} \quad \text{and} \quad \eta_m = \frac{\bar{H} \cdot \bar{n}}{2\pi}$$

$$M_1' = M_2' = \frac{4}{3} a^3 \quad \dots \text{?c}^*$$

$$P' = \frac{2}{3} a^3 \quad \dots (71)$$

$$\bar{x}' = -\frac{M_1'}{2\pi} \bar{H}_0 \quad (\text{emu})$$

M.K.S. from § 7 this means:

$$N = N' \mu_0 \quad \mu_0 = 4\pi \times 10^{-7}$$

$$\frac{M_1}{N} = \frac{M_2}{N} = \frac{4}{3} a^3 \quad (81)^*$$

$$\frac{P}{E} = \frac{2}{3} a^3 \quad (82)$$

$$\bar{x} = -M_1 H_0 \quad (\text{webermeter})$$

+ These two different methods of dividing the problem into left and right halves are consistent as far as the solution for $\bar{E} \times \bar{n}$ and $\bar{H} \cdot \bar{n}$ in the aperture. The definition by Bethe of $\eta_m = 2 \left(\frac{\bar{H} \cdot \bar{n}}{4\pi} \right)$ appears to put an extra factor of 2 into the magnetic and electric moments.

* From dimensional analysis one could guess: $\frac{M}{N} = \frac{4\pi}{2\pi} \frac{M'}{N'} = 2 \dots$

The difference in the two definitions should be resolved by dividing the

$$\left(\frac{M}{N'} = \frac{1}{\text{not } 2.} \right) \text{ is that:}$$

Both apparently split the problem into two symmetrical parts. The

H_{2tan} by 2 after (11.5) by using $\eta_m = \frac{\bar{H} \cdot \bar{n}}{2\pi}$ not $\eta_m = \frac{\bar{H} \cdot \bar{n}}{4\pi}$ in the

paper the equivalent definition is $\eta_m = \frac{\bar{H} \cdot \bar{n}}{2\pi}$ by 2 at (11.5).

Check against results for μ_0 and μ_0 if μ_0 is around a factor

Wang's μ_0 is $\frac{4\pi}{2\pi} \mu_0 = 2 \mu_0$ the result for other cases is

transposed from Bethe's Gaussian system which is consistent with the other

b. Circular Aperture.

Both papers give $\mu_0 = 4\pi \times 10^{-7}$ webermeter

inside an elliptic window, which is to the following:

a = major axis b = minor axis

eccentricity $E = \sqrt{1 - \left(\frac{b}{a}\right)^2}$ (84a)

F, E are complete elliptic integrals:

$$F = F(E) = \int_0^{\pi/2} \frac{d\phi}{\sqrt{1 - E^2 \sin^2 \phi}} \quad E = E(E) = \int_0^{\pi/2} \sqrt{1 - E^2 \sin^2 \phi} \quad (85)$$

$$\frac{M_1}{N} = \frac{\pi a b^2 E^2}{3(1-E^2)(E-E)} \quad \frac{M_2}{L} = \frac{\pi a^2 E^2}{3(E-(1-E^2))} \quad \frac{P}{E} = \frac{\pi}{3} \quad (86)$$

For small E : $E \approx \frac{\pi}{2} [1 - \frac{1}{2} E^2]$ (87a) $F \approx \frac{\pi}{2} [1 + \frac{1}{4} E^2]$ (87b)
 from which it can be seen that (E^2) values
 (80, 81) for $a = a$.

For large E ($a \rightarrow b$): $E \rightarrow 1$; $F \rightarrow b/a \sqrt{1-E^2}$ (88)

Elliptical slit ($E = 1$)
 $\frac{M_1}{N} = \frac{\pi}{3} \ln \left(\frac{a+b}{a-b} \right) - 1$ (87a) $\frac{L}{N} = \frac{\pi}{3} a b^2$ (87b) $\frac{P}{E} = \frac{\pi}{3} a b^2$ (87c)

d. Rectangular slit (87d)

Let $a = d$



For a rectangular slit, the eccentricity E is defined as $E = \sqrt{1 - \left(\frac{b}{a}\right)^2}$. For a rectangular slit, $a = d$ and $b = h$. The eccentricity E is then $E = \sqrt{1 - \left(\frac{h}{d}\right)^2}$. The complete elliptic integrals F and E are functions of E . The integrals F and E are defined as $F = \int_0^{\pi/2} \frac{d\phi}{\sqrt{1 - E^2 \sin^2 \phi}}$ and $E = \int_0^{\pi/2} \sqrt{1 - E^2 \sin^2 \phi} d\phi$. The integrals F and E are used to calculate the moments M_1 and M_2 and the area P of the slit.

$$\frac{P}{E} = \frac{4d^2}{\pi} = \frac{P}{16} (d^2)$$

The area P of the slit is $P = d h$. The area P is used to calculate the moments M_1 and M_2 . The moments M_1 and M_2 are used to calculate the center of mass of the slit. The center of mass is the point where the slit would balance if it were suspended from that point.

$$\frac{M_1}{N} = \frac{P}{16} = \frac{d h}{16}$$

$$\frac{M_2}{L} = \frac{P}{16} = \frac{d h}{16}$$

9. The Poynting Vector.

The time average Poynting vector: $S = \frac{1}{2} \text{Re}(\bar{E} \times \bar{H}^*)$ Integrating over the aperture and using peak values of E, H , since time factors cancel out

$$(90) \quad S = \frac{1}{2} \int_{n_s} \bar{E}_1 \times \bar{H}_1 \cdot \bar{n} \, dS$$

\bar{E}_1, \bar{H}_1 are fields generated in aperture by incident field \bar{E}_0, \bar{H}_0 .

If we resolve the diffraction field on the right into normal modes, then

for mode i ,

$$(91) \quad S_i = \frac{1}{2} \int \bar{E}_1 \times \bar{H}_{2i} \cdot \bar{n} \, dS$$

$\bar{E}_{2i}, \bar{H}_{2i}$ are fields of the normal mode to be excited on the right. \bar{E}_2 is obtained from the theory of waveguide resonators. We now use the theory of the first part of this paper to let \bar{H}_2 in terms of \bar{E}_0, \bar{H}_0 . We first expand \bar{H}_2 in about e.g. in a Taylor series

$$\bar{H}_2 = \bar{H}_2(0) + (\bar{r} \cdot \nabla) \bar{H}_2 + \dots$$

Keeping only first two terms since $(\bar{r} \cdot \nabla) \bar{H}_2 = S_1 + S_2$ where

$$(4+) \quad \begin{aligned} S_1 &= \frac{1}{2} \int \bar{E}_1 \times \bar{H}_2(0) \cdot \bar{n} \, dS = \frac{1}{2} \int (\bar{n} \times \bar{E}_1) \cdot \bar{H}_2(0) \, dS = \\ S_1 &= \frac{1}{2} \bar{H}_2(0) \cdot \int \bar{n} \times \bar{E}_1 \, dS = \frac{1}{2} \omega [M_1 H_{0e} H_{2e} + M_2 H_{0m} H_{2m}] \\ S_2 &= \frac{1}{2} \int (\bar{n} \times \bar{E}_1) \cdot (\bar{r} \cdot \nabla) \bar{H}_2 \, dS \end{aligned} \quad (93)$$

$$\bar{r} \cdot \nabla = x \frac{\partial}{\partial x} + y \frac{\partial}{\partial y} \quad \text{so} \quad S_2 = \frac{1}{2} \int \left\{ E_{1y} \left(r \frac{\partial H_{2x}}{\partial x} + y \frac{\partial H_{2y}}{\partial y} \right) + E_{1x} \left(x \frac{\partial H_{2y}}{\partial x} + y \frac{\partial H_{2x}}{\partial y} \right) \right\} dS$$

Part of the terms integrate to zero as in (49).

$$S_2 = \frac{P}{\epsilon} \left(\frac{\partial H_{2x}}{\partial x} \frac{\partial H_{2y}}{\partial y} \right) \quad \text{by (49)} \quad S_2 = \frac{1}{2} P E_{0m} E_{2m}$$

$$(12)(94) \quad \boxed{S = S_1 + S_2 = \frac{1}{2} [M_1 H_{0e} H_{2e} + M_2 H_{0m} H_{2m} + P E_{0m} E_{2m}]}$$

in general E_n and H_{tan} are 90° out of phase so that $E_{on} \cdot E_{2n}$ is negative when H_0, H_2 is positive.

Although Bethe's development is in gaussian units, there is no $\frac{c}{4\pi}$ in his Poynting vector, Ref. 2, eq. 51. It is safer to start from the beginning in M. K. S. units, than to transform Bethe's formulas to M. K. S. units. The factor $\frac{c}{4\pi}$ does appear correctly ⁱⁿ Ref. 2, eq. 6.

10. Change of Resonant Frequency of Cavity.

From Bethe and Schwinger's² perturbation theory for cavities, the shift in resonant frequency of a resonator due to a small window is:

$$(96) \quad \Delta k = k_1 - k_2 = \frac{\int \bar{E}_1 \times \bar{H}_2' \cdot \bar{n} \, dS}{\int (\epsilon E_2^2 - \mu H_2'^2) \, dV} \quad (\text{GAUSSIAN})$$

Transforming to M.K.S. units and checking with (3) p. 81_A for consistency: ⁽⁹⁶⁾ ^{eq. (7.1)}

$$(96a) \quad \omega_1 - \omega_2 = \frac{\frac{1}{2} \int \bar{E}_1 \times \bar{H}_2' \cdot \bar{n} \, dS}{\frac{1}{2} \int (\epsilon E_2^2 - \mu H_2'^2) \, dV} \quad (\text{M.K.S.})$$

Although the results calculated from this agree with experimental values, this development should be checked.

$$(96b) \quad H_2 = +jH_2' \quad \omega_1 - \omega_2 = \frac{S}{\frac{1}{2} \int (\epsilon E_2^2 + \mu H_2'^2) \, dV} \quad (96c)$$

$$(97) \quad \frac{\Delta \omega}{\omega} = \frac{\frac{1}{2} [P_{in} E_{2m} + jM_1 H_2' + jM_2 H_2'']}{\int (\epsilon E_2^2 + \mu H_2'^2) \, dV}$$

This is for a resonant cavity with a source of energy inside radiating out through the window where no energy is reflected back toward the cavity. Practically it is supposed to be good as long as the external incident wave or reflected wave has $V \Delta t \ll \frac{\omega}{\Delta \omega}$. Since \bar{E}_0, \bar{H}_0 is the field of the cavity itself and is identical with \bar{E}_2, \bar{H}_2 we have:

$$(97a) \quad \frac{\Delta \omega}{\omega} = \frac{P E_{2m}^2 - M_1 H_2'^2 - M_2 H_2''^2}{\int (\epsilon E_2^2 + \mu H_2'^2) \, dV}$$

From Bethe and Schwinger² or from 81_A ²⁶ the increase of volume of a resonant cavity is:

$$(97b) \quad \frac{\Delta \omega}{\omega} = \frac{(\epsilon E^2 - \mu H^2) \Delta V}{\int (\epsilon E^2 + \mu H^2) \, dV}$$

Comparison with (9 a) shows that $\frac{P}{E} \frac{M_1}{N}, \frac{M_2}{N}$ represent the effective increase in volume due to a window in a cavity.

Sample calculation of $\frac{\Delta \omega}{\omega}$ from experimental data of F. R. Wood:²⁹

Brass TM_{020} resonator. Dimensions are shown in figure on page 331.

$$\frac{M_1}{N} = \frac{\pi d^2}{16} \quad k_c = \frac{2.02}{a} = \frac{5.52}{a} \quad \eta_1 = \sqrt{\frac{N}{E}}$$

$$E_z = E_0 J_0(k_c r) \quad H_\theta = j \frac{E_0}{\eta_1} J_1(k_c r)$$

$$\text{stored Energy: } U_E = \int \frac{\epsilon E^2}{2} dv = \pi \epsilon h E_0^2 \frac{a^2}{2} J_0^2(k_c a)$$

$$\text{By (17a)} \quad \frac{\Delta \omega}{\omega} = - \frac{M_1 |H_\theta|^2}{\int (\epsilon E^2 + \mu H^2) dv} = - \frac{M_1 |H_\theta|^2}{2 \int \epsilon E^2 dv}$$

$$\frac{\Delta \omega}{\omega} = - \frac{M_1 |H_\theta|^2}{4 U_E} = - \frac{\left(\frac{\pi \mu h d^2}{16} \right) \left(\frac{E_0^2}{\eta_1^2} \right) J_1^2(k_c a)}{4 \pi \epsilon h E_0^2 \frac{a^2}{2} J_0^2(k_c a)}$$

$$\frac{\Delta \omega}{\omega} = - \frac{1}{32} \left(\frac{d}{a} \right)^2$$

d''	d/a	$(d/a)^2$	$-\frac{1}{32} \left(\frac{d}{a} \right)^2$	$\left(\frac{\Delta \omega}{\omega} \right)_{exp.}$
.125	.109	.0128	-.0004	-.00036
.250	.218	.047	-.0015	-.0014
.500	.435	.19	-.0059	-.0054

a = radius of resonator

d = width of window

11. Susceptance of Iris in Waveguide.

a. General Case:

We consider a waveguide of arbitrary cross-section with metal diaphragm extending across it having a small window. The excitation on the left is given and it is assumed that there is no strong reflected wave coming back from right. The exciting field on left may be in (1) waveguide of same cross-section, (2) waveguide of different cross-section (3) free space, or (4) a resonant cavity.

From Silver³⁰ or Pothe³¹, the normal modes in the waveguide on the right are:

$$\begin{aligned} \vec{E}_t &= \sum_a A_a \vec{E}_{at} e^{-j\gamma_a z} & (98) & \quad \vec{E}_z = +j \sum_a A_a E_{am} e^{-j\gamma_a z} & (98a) \\ \gamma_a &= 2\pi/\lambda_g & (98b) & \quad \vec{H}_z = +j \sum_a A_a H_{am} e^{-j\gamma_a z} & (98d) \\ \vec{H}_t &= \sum_a A_a \vec{H}_{at} e^{-j\gamma_a z} & (98c) & \end{aligned}$$

The amplitude factor is: $A_a = S_{\text{hole}} / S_{\text{subwaveguide } a}$.

From (98)(98a)(98b)(98c)(98d):

$$(99) \quad A_a S_a = \frac{1}{2} \int_{\text{hole}} \vec{E}_1 \times \vec{H}_{at} \cdot \vec{n} \, dS$$

$$(100) \quad S_a = \frac{1}{2} \int_{\text{guide cross}} \vec{n} \times \vec{E}_a \cdot \vec{H}_a \, dS$$

$$(101) \quad A_a = \frac{j\omega}{2S_a} [M_1 H_{0z} (H_{1z}) + M_2 H_{0z} H_{2zm} + j P E_{0z} E_{2z}]$$

b. Excitation of same cross-section on both sides.

Assume that the diaphragm is such that only one normal mode b is excited on the left. Let $A_b = 1$ for incident wave. E_y, H_z odd, while E_x, H_y even.

$$(102) \quad \vec{H}_t = \vec{H}_{at} (e^{-j\gamma_b z} + R e^{j\gamma_b z}) = 2 \vec{H}_{at} \cos \gamma_b z$$

$$(103) \quad \vec{H}_{0z} = 2 A_b H_{0z} \quad \text{and} \quad \vec{E}_{0z} = +2j E_{0z} \quad \text{at } z=0$$

by
 (102) in (101):
 (103)
$$A_a = -\frac{2j\omega}{2S_a} [P E_{im} E_{am} - M_1 H_{ae} H_{ae} - M_2 H_{am} H_{am}]$$

From (103) we can compute the amplitude of each possible mode on the right.

In this case there is only one, i.e. $a = b$, so:

(104)
$$A_a = -\frac{2j\omega}{2S_a} (P E_{im}^2 - M_1 H_{ae}^2 - M_2 H_{am}^2)$$

The susceptance B (for $V_0 = 1$) of an iris is related to the transmission

coefficient by:
$$A_a = \frac{1}{1 + j \frac{B}{Z}} \quad (105)$$

For small A_a :

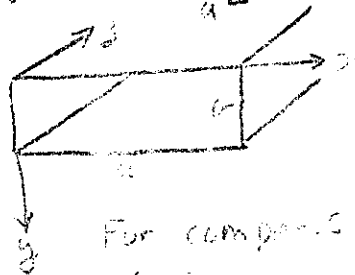
By (104)(105):

(106)

$$\frac{1}{B} = \frac{\omega}{2S_a} (P E_{im}^2 - M_1 H_{ae}^2 - M_2 H_{am}^2) \quad (105a)$$

c. Iris in TE₁₀ Waveguide.

$$\gamma^2 = k^2 - \frac{\pi^2}{a^2}$$



$$E_{xy} = A \frac{k}{\gamma} \sin \frac{\pi x}{a}$$

$$H_{xz} = -A \sqrt{\frac{\epsilon}{\mu}} \sin \frac{\pi x}{a}$$

$$H_{yz} = +j \frac{\pi}{a} \frac{A}{\gamma} \sqrt{\frac{\epsilon}{\mu}} \cos \frac{\pi x}{a}$$

(107)

For comparison this corresponds to treatment of Ramo and Whinnery³² when $B = j \frac{\pi}{a} \frac{A}{\gamma} \sqrt{\frac{\epsilon}{\mu}}$

(108)(107)
$$S_a = \frac{1}{2} \int_{\text{guide}} (\vec{\alpha} \times \vec{E}_0) \cdot \vec{H}_0 dS = A^2 \frac{ab}{4} \frac{k}{\gamma} \sqrt{\frac{\epsilon}{\mu}} \quad (108a)$$

By (108a)

(108)(107):
$$B \frac{1}{B} = -\frac{ab \lambda_g}{4\pi \left(\frac{\mu_0}{\mu}\right) \sin^2 \frac{\pi x}{a}} \quad (108b)$$

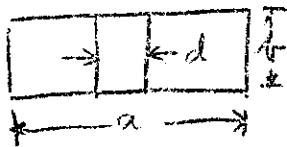
9/9/52
 779

From $E_{0y} = 0$, $H_{ae} = H_{ax} \cos(\vec{E}, \vec{x})$, $H_{am} = H_{ax} \sin(\vec{E}, \vec{x})$

in
$$\frac{1}{B} = -\frac{2\gamma}{ab} \frac{1}{j} \frac{\sin^2 \frac{\pi x_0}{a}}{a} [M_1 \cos^2(\vec{E}, \vec{x}) + M_2 \sin^2(\vec{E}, \vec{x})] \quad (108c)$$

x_0 = distance to c.g. of slit

For an inductive slit, $\chi_0 = \frac{\pi}{2}$ by (88) in (1084)



$$\frac{B}{Y_0} \frac{d}{a} = - \frac{4}{\pi^2} \left(\frac{a}{d} \right)^2 \quad (1090)$$

From the Waveguide Handbook³³ we obtain a more precise solution (for comparison (derived in gaussian units, but requires no change for M.K.S. since it is a dimensionless ratio))

$$\left| \frac{Y_0}{B} \frac{d}{a} \right| = \tan^2 \frac{\pi d}{2a} \left\{ 1 + \frac{2}{\pi} \sin^2 \frac{\pi d}{a} \left(\frac{1}{\sqrt{1 - \left(\frac{2d}{a} \right)^2}} - 1 \right) + 2 \left(\frac{a}{\lambda} \right)^2 \left[- \frac{4}{\pi} \frac{E(\Delta) - \Delta^2 F(\Delta)}{\Delta^2} \frac{E(\Delta) - \Delta^2 F(\Delta)}{\Delta^2} - \frac{1}{\pi} \operatorname{arcsin} \frac{\Delta}{a} \right] \right\}$$

$$\Delta = \sin \frac{\pi d}{2a} \quad \Delta' = \cos \frac{\pi d}{2a} \quad E, F \text{ are elliptic integrals} \quad (1091)$$

$$\text{For small } \frac{d}{a}: \left| \frac{Y_0}{B} \frac{d}{a} \right| \approx \tan^2 \frac{\pi d}{2a} \rightarrow \frac{\pi}{4} \left(\frac{d}{a} \right)^2 \quad (1092)$$

Comparing (1092) with (1090) we see that they are the same. The curves are plotted in Figures 1 and 2. See also Fig. 2.11A-14B

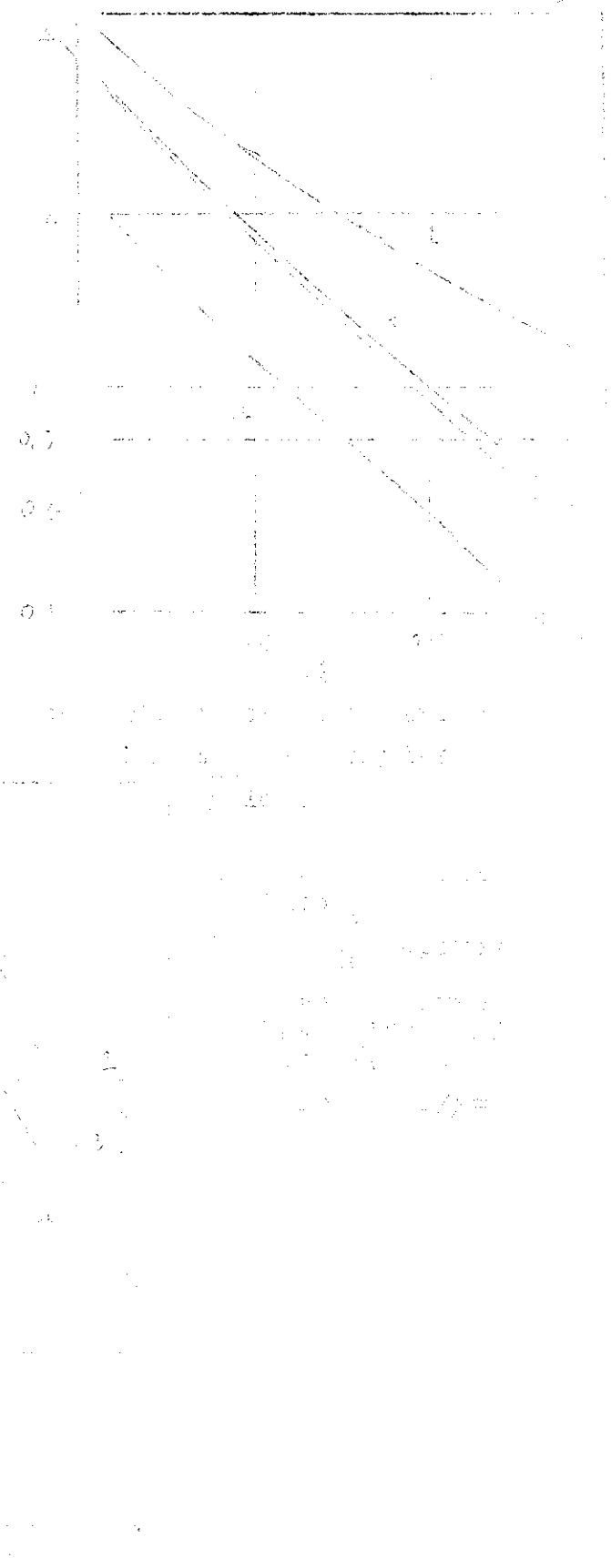
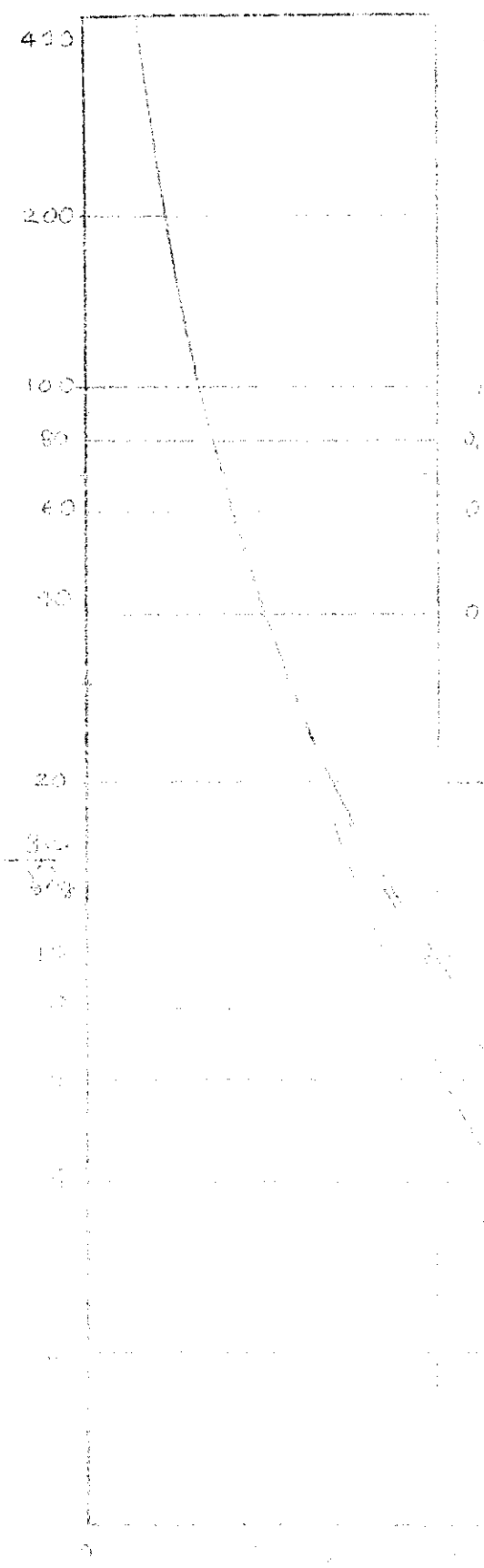
(1) Small hole theory of Fig. 1 is (1090)

(2) $\cot^2 \frac{\pi d}{2a}$ approximation

(3) Curves from (1091) are curves in (1092)³³ of $\chi_0 = 0$

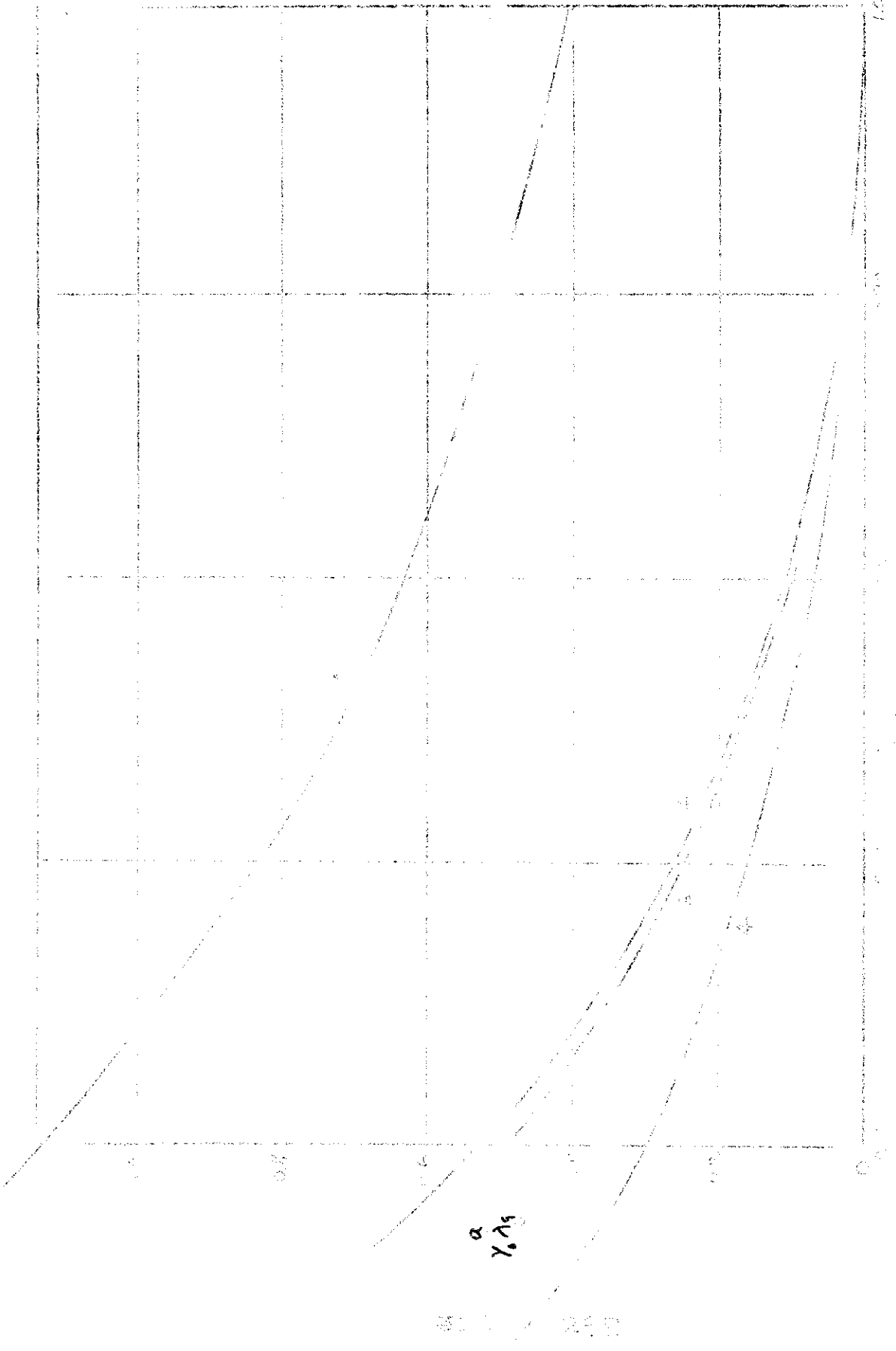
(4) Curves from (1091) are curves in (1092)³³ of $\chi_0 = \frac{\pi}{2}$

Approximate³⁴ by for a further check on the susceptibility of iris in waveguides using the method of residues developed by Schlinger.



(cont. from p. 100)

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12. Energy Emitted from a Cavity Through Window into Free Space.

Bethe's² equations (3) and (4) are not consistent with (13a)(25) by a constant $(27)^2$. This makes his equation (4) give an energy emitted that is 40.6 times the correct value. In all assumptions and definitions at the beginning of his paper are correct.

Have we started with Strahlungsdruck of the radiation from electric and magnetic dipoles? Here is a correction to correct those equations should be divided by 3 since they are half wave length right to left considered. It goes on to show that if change to get received as the application into the right direction of the radiation of \vec{E} and \vec{H} with a constant $(27)^2$.

$$S = \frac{1}{12\pi} \int_{\Omega} (E^2 + N^2) d\Omega$$

(110) $S = \frac{\omega^4}{12\pi} \int_{\Omega} (E^2 + N^2) d\Omega$

By (43) (110) $S = \frac{4\pi}{3} \int_{\Omega} \frac{1}{2} (E^2 + N^2) d\Omega$

Now that we have the radiation field we can calculate the radiation pressure on a surface perpendicular to the direction of propagation of the radiation.

$$\frac{1}{Q_c} = \frac{1}{4\pi} \int_{\Omega} \frac{E^2 + N^2}{E^2 + N^2} d\Omega = \frac{1}{4\pi} \int_{\Omega} (E^2 + N^2) d\Omega$$

(111a) $\frac{1}{Q_c} = \frac{4\pi}{12\pi} \int_{\Omega} (E^2 + N^2) d\Omega$

(111b) $\frac{1}{Q_c} = \frac{4\pi}{12\pi} \frac{\epsilon (\frac{P}{\epsilon})^2 E_{0n}^2 + N \left\{ (\frac{M_1}{N})^2 H_{0n}^2 + (\frac{M_2}{\epsilon})^2 H_{0m}^2 \right\}}{\int (\epsilon E^2 + N^2) dV}$

Sample calculation on cavity resonator shown on p. 26 and 33.

from (111b) $\frac{1}{Q_c} = \frac{k^3}{12\pi} \frac{N \left(\frac{H_0}{E}\right)^2 |H_{01}|^2}{U_{E_{0000}}} = \frac{k^3 \pi^2 h^2 d^2 E_0^2 J_1^2(k_0 a)}{12\pi \cdot 256 \eta_1^2 \pi^2 E h E_0^2 \frac{1}{2} J_1^2(k_0 a)}$

$$\frac{1}{Q_c} = \frac{16\pi^2}{12 \cdot 256} \frac{h d^2}{a^2 \lambda^2} \quad Q_c = \frac{192}{\pi^2} \frac{a^2 \lambda^2}{h d^2} \quad (111c)$$

for TM_{020} resonator with $a = 100 \text{ cm}$, $b = 1 \text{ cm}$, $d = 3 \text{ cm}$

$$Q_c = \frac{192}{\pi^2} \frac{100^2 \cdot 100^2}{(3)^2} = \frac{576}{\pi^2} \quad (111d)$$

The quality factor Q_c is a measure of the energy stored in the resonator relative to the energy dissipated per cycle. It is defined as $Q_c = \frac{\text{Energy stored}}{\text{Energy dissipated per cycle}}$. For a resonator, the quality factor is related to the bandwidth of the resonance. A high Q_c indicates a narrow resonance bandwidth, while a low Q_c indicates a broad bandwidth. In the context of a resonator, the quality factor is also related to the decay time of the stored energy. A high Q_c corresponds to a long decay time, while a low Q_c corresponds to a short decay time. The quality factor is a dimensionless quantity and is typically denoted by the symbol Q or Q_c . In the case of a resonator, the quality factor is often denoted by Q_c to distinguish it from the quality factor of a single mode. The quality factor is a key parameter in the design of resonators and is used to characterize their performance. A high quality factor is desirable for many applications, as it allows for the storage of energy for a long time with minimal loss. The quality factor is also used to determine the bandwidth of a resonator, which is the range of frequencies over which the resonator can operate effectively. The quality factor is a function of the geometry of the resonator and the material properties of the resonator walls. In the case of a cylindrical resonator, the quality factor is a function of the radius, length, and wall thickness of the resonator. The quality factor is also a function of the frequency of the resonance. In general, the quality factor increases with the frequency of the resonance. The quality factor is a key parameter in the design of resonators and is used to characterize their performance. A high quality factor is desirable for many applications, as it allows for the storage of energy for a long time with minimal loss. The quality factor is also used to determine the bandwidth of a resonator, which is the range of frequencies over which the resonator can operate effectively. The quality factor is a function of the geometry of the resonator and the material properties of the resonator walls. In the case of a cylindrical resonator, the quality factor is a function of the radius, length, and wall thickness of the resonator. The quality factor is also a function of the frequency of the resonance. In general, the quality factor increases with the frequency of the resonance.

13. Energy Emitted Through Window into Waveguide.

The normal modes in the waveguide are given by (98). The Poynting

vector is:
$$S = \frac{1}{2} \int \vec{E} \times \vec{H}^* \cdot \vec{n} dS \quad (10)$$

$$S = \frac{1}{2} \int \left(\sum_a A_a \vec{E}_{0a} e^{-j\beta_a z} \right) \cdot \left(\sum_a A_a \vec{H}_{0a} e^{+j\beta_a z} \right) dS =$$

$$(11) \quad S = \frac{1}{2} \sum_a |A_a|^2 \int \vec{E}_a \times \vec{H}_a^* \cdot \vec{n} dS = \frac{1}{2} \sum_a |A_a|^2 S_a$$

$$(11) \quad S_a = \sum_n \frac{\omega^2}{2} |M_n|^2 \left(H_{0n}^2 + H_{0n} H_{0m} + j P E_{0n} E_{0m} \right)$$

In general there can be interference between various components of electric and magnetic current of the window in connection to radiation into free space.

For a certain window field $\vec{H}_0 = \vec{H}_0^*$ where \vec{H}_0 and \vec{H}_0^* are real.

$$(12) \quad S = \frac{\omega^2}{2} \sum_n |M_n|^2 \left(H_{0n}^2 + H_{0n} H_{0m} + j P E_{0n} E_{0m} \right)$$

It would appear from the above that there should be a relation between the Poynting vector and the field (9) to be considered in (12).

Consider the case of a thin window.

$H_{0e} = H_{0c}$ is the only magnetic component in (9).

$$(13) \quad S = \frac{\omega^2}{2} \sum_n |M_n|^2 \left(H_{0n}^2 + H_{0n} H_{0m} + j P E_{0n} E_{0m} \right) \quad (13)$$

For a window $M_n = M_1 = \frac{P}{\omega} \frac{H_{0n}^2}{2}$ (14)

$$(14) \quad S = \frac{\omega^2}{2} \sum_n |M_n|^2 \left(H_{0n}^2 + H_{0n} H_{0m} + j P E_{0n} E_{0m} \right) = \frac{\omega^2}{2} \sum_n \left(\frac{P^2}{\omega^2} \frac{H_{0n}^4}{4} + \dots \right)$$

$$\therefore \frac{S}{\omega^2} = \frac{P^2}{2} \sum_n \frac{H_{0n}^4}{4} + \dots = \frac{S}{\omega^2} = \frac{S}{\omega^2} \frac{1}{2} \sum_n \frac{H_{0n}^4}{4}$$

$$\frac{1}{Q_c} = \frac{\omega^2}{2} \frac{P^2}{\omega^2} \frac{M_1^2}{\omega^2} \frac{H_{01}^4}{4} + \dots = \frac{\omega}{2} \frac{P}{\omega} \frac{P}{\omega} \frac{M_1^2}{\omega^2} \frac{H_{01}^4}{4} + \dots$$

$$(15a)(98) \quad \frac{1}{Q_c} = \frac{1}{2L} \frac{\gamma}{\sqrt{\mu \epsilon}} \frac{1}{4\pi} \frac{N^2 \pi^2 \lambda}{253 \pi \epsilon} \frac{\epsilon^2}{R \epsilon^2} \left(\frac{\epsilon}{P}\right)^2$$

$$Q_c = \frac{2L}{\pi^2} \frac{R^2 \epsilon^2 \lambda \epsilon}{R \epsilon^2} \quad (116)$$

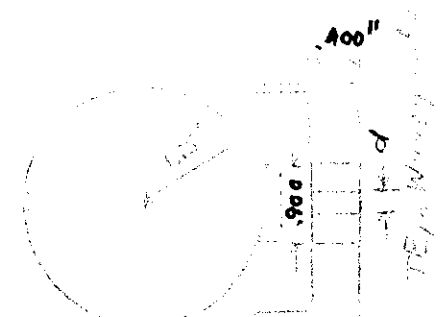
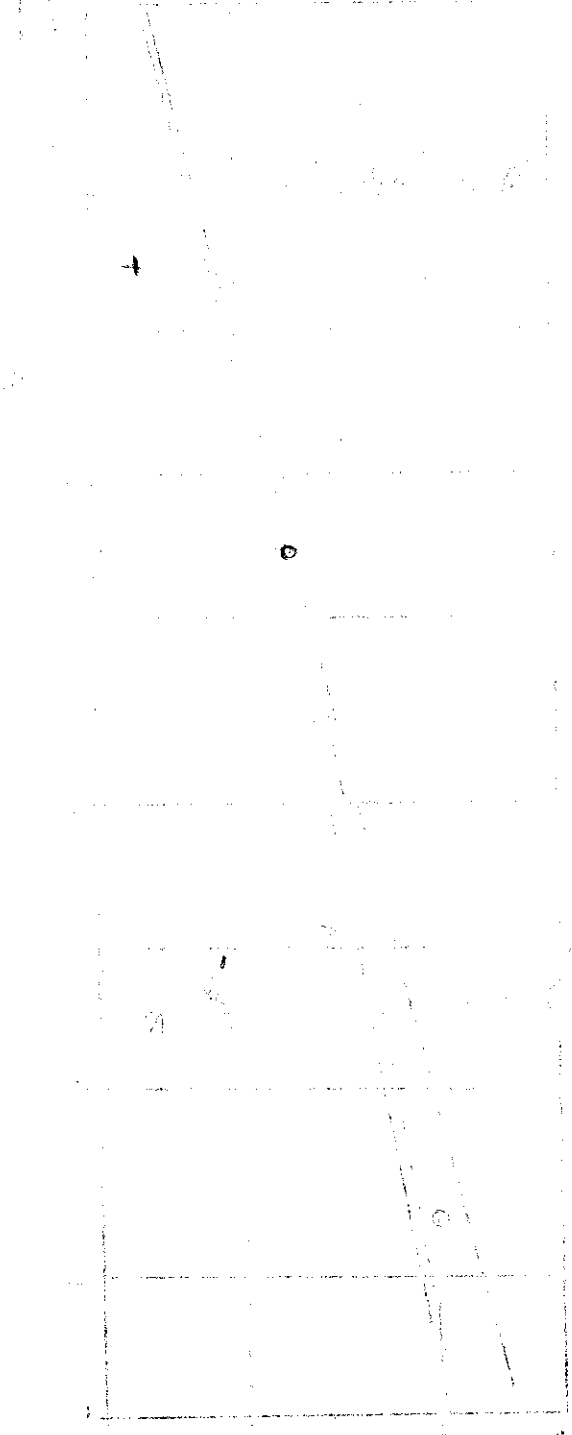
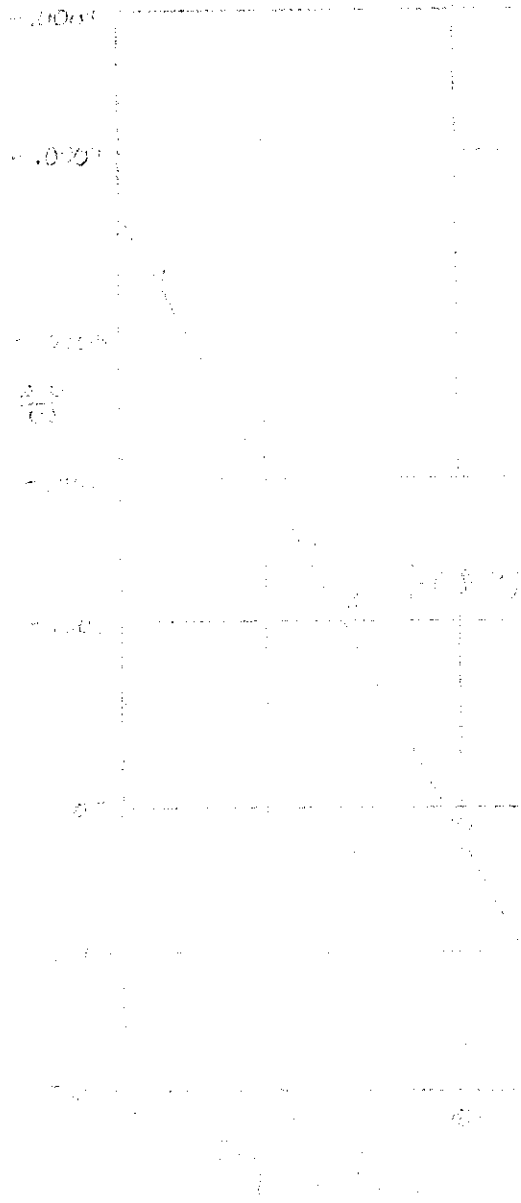
For TM₀₂₀ resonator; $\lambda = 3.35 \mu\text{m}$, $\epsilon = 2.93$ (see table 4)
 $\lambda = 3.35 \mu\text{m}$, $\epsilon = 2.93$ (see table 4)

$$Q_c = \frac{120}{\pi^2} \frac{R^2 \epsilon^2 \lambda \epsilon}{R \epsilon^2} = \frac{120}{\pi^2} \frac{R^2 \epsilon^2 \lambda \epsilon}{R \epsilon^2} = \frac{120 \epsilon^2 \lambda \epsilon}{\pi^2 R \epsilon^2}$$

R (cm)	Q_c	A_{eff} (cm ²)	η_{eff} (dB)	β_{eff} (rad)
1.25	12,000	100 (10)	3 (10)	$(2.93 \times 10^{-2})^2$
1.25	12,000	100 (10)	3 (10)	$(2.93 \times 10^{-2})^2$
1.25	12,000	100 (10)	3 (10)	$(2.93 \times 10^{-2})^2$
1.25	12,000	100 (10)	3 (10)	$(2.93 \times 10^{-2})^2$

Table 4: Summary of parameters for the resonator. The table lists the radius R in cm, the quality factor Q_c , the effective area A_{eff} in cm², the effective loss η_{eff} in dB, and the effective phase β_{eff} in rad. The values for A_{eff} and η_{eff} are constant across all entries, while Q_c and β_{eff} vary with R .

Comparison of ... with ...



iris width (inches)

APPE 308 - Units and Definitions.

Rev.	Unit	Definition	Notes
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APPENDIX 7 - FORM 10 PART II - of 10/1/1993

The following information is to be provided in the form of a written report to the Board of Directors of the Corporation, and shall be included in the annual report of the Corporation to its stockholders, and shall be made available to the public in accordance with the provisions of the Securities Exchange Act of 1934, as amended, and the rules and regulations thereunder.

by

APPENDIX 1 - THE NATIONAL ANTHROPOLOGICAL ARCHIVES - PROCEEDINGS OF THE BOARD OF DIRECTORS

The Board of Directors of the American Anthropological Association met in Washington, D.C., on the 18th and 19th of December, 1954. The meeting was held in the American Anthropological Association building, 1201 Constitution Avenue, N.W., Washington, D.C. The meeting was presided over by the President of the Association, Dr. [Name].

The following is a summary of the proceedings of the meeting. The Board of Directors met in regular session on the 18th of December, 1954, at 10:30 a.m. The meeting was called to order by the President, Dr. [Name]. The minutes of the previous meeting were read and approved. The following items were discussed and action was taken:

- s
- t
- 1. Report of the President, Dr. [Name].
- 2. Report of the Vice-President, Dr. [Name].
- 3. Report of the Secretary, Dr. [Name].
- 4. Report of the Treasurer, Dr. [Name].
- 5. Report of the Executive Committee.
- 6. Report of the Board of Directors.
- 7. Report of the Committee on the [Topic].
- 8. Report of the Committee on the [Topic].
- 9. Report of the Committee on the [Topic].
- 10. Report of the Committee on the [Topic].

The Board of Directors also held a special session on the 19th of December, 1954, at 10:30 a.m. The meeting was called to order by the President, Dr. [Name]. The following items were discussed and action was taken:

APPENDIX B - EFFECT OF FINITE THICKNESS
OF SCREEN.

For small width holes the effect of the finite thickness of the resonator wall becomes important. Curves are available for the change in the power emitted in waveguide in terms of the hole susceptance of equivalent network in the transmission line for a circular aperture, ¹ since the corresponding resonator Q factor readily available for rectangular holes, the calculation is made as follows:

$$Q = \frac{2\pi \epsilon_0 \epsilon_r \omega \mu_0 \epsilon_0 \epsilon_r}{\frac{1}{\omega} \left(\frac{1}{Z_{in}} + \frac{1}{Z_{out}} \right)}$$

where Z_{in} thickness
 $Z_{out} = \frac{1}{\omega} \sqrt{\epsilon_0 \epsilon_r (1 - \beta^2)}$

It can be seen that the Q factor is a function of the hole diameter and the resonator length. The Q factor is a function of the hole diameter and the resonator length.

$$Q = \frac{2\pi \epsilon_0 \epsilon_r \omega \mu_0 \epsilon_0 \epsilon_r}{\frac{1}{\omega} \left(\frac{1}{Z_{in}} + \frac{1}{Z_{out}} \right)}$$

for $\beta \ll 1$, $Z_{out} \approx \frac{1}{\omega} \sqrt{\epsilon_0 \epsilon_r}$

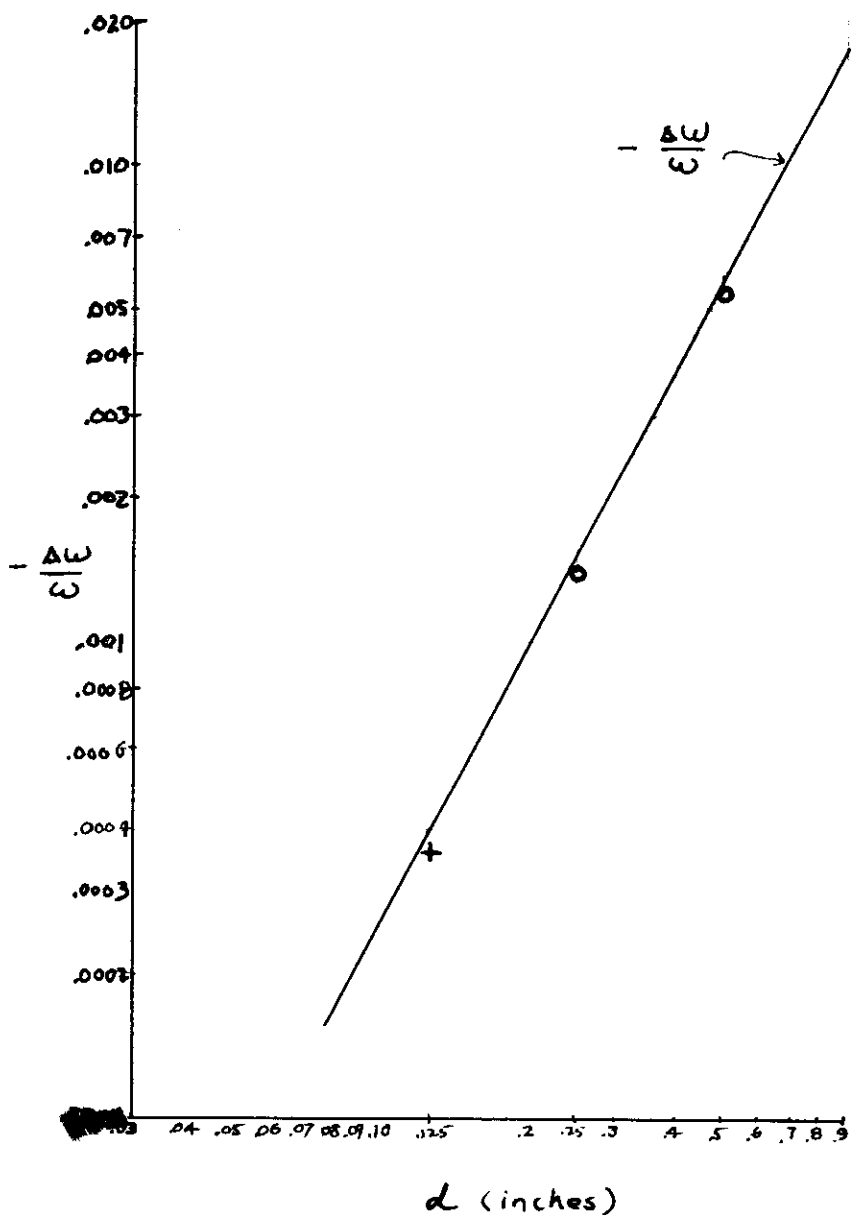
$G_2 = \frac{1}{\omega} \sqrt{\epsilon_0 \epsilon_r}$

For a given hole diameter and resonator length, the correction applied to the Q factor is tabulated.

f	λ_{cm}	$\frac{d}{\lambda_{cm}}$	$\frac{L}{\lambda_{cm}}$	Q_{cm}	$2\pi d$	$e^{2\pi d}$	Q_{corr}
8951	3.17	0.07	0.50	6.07	1.00	3.96	3.17
8943	3.22	0.11	0.50	12	0.82	1.77	3.17
8925	3.27	0.15	0.50	18	0.60	1.07	3.17

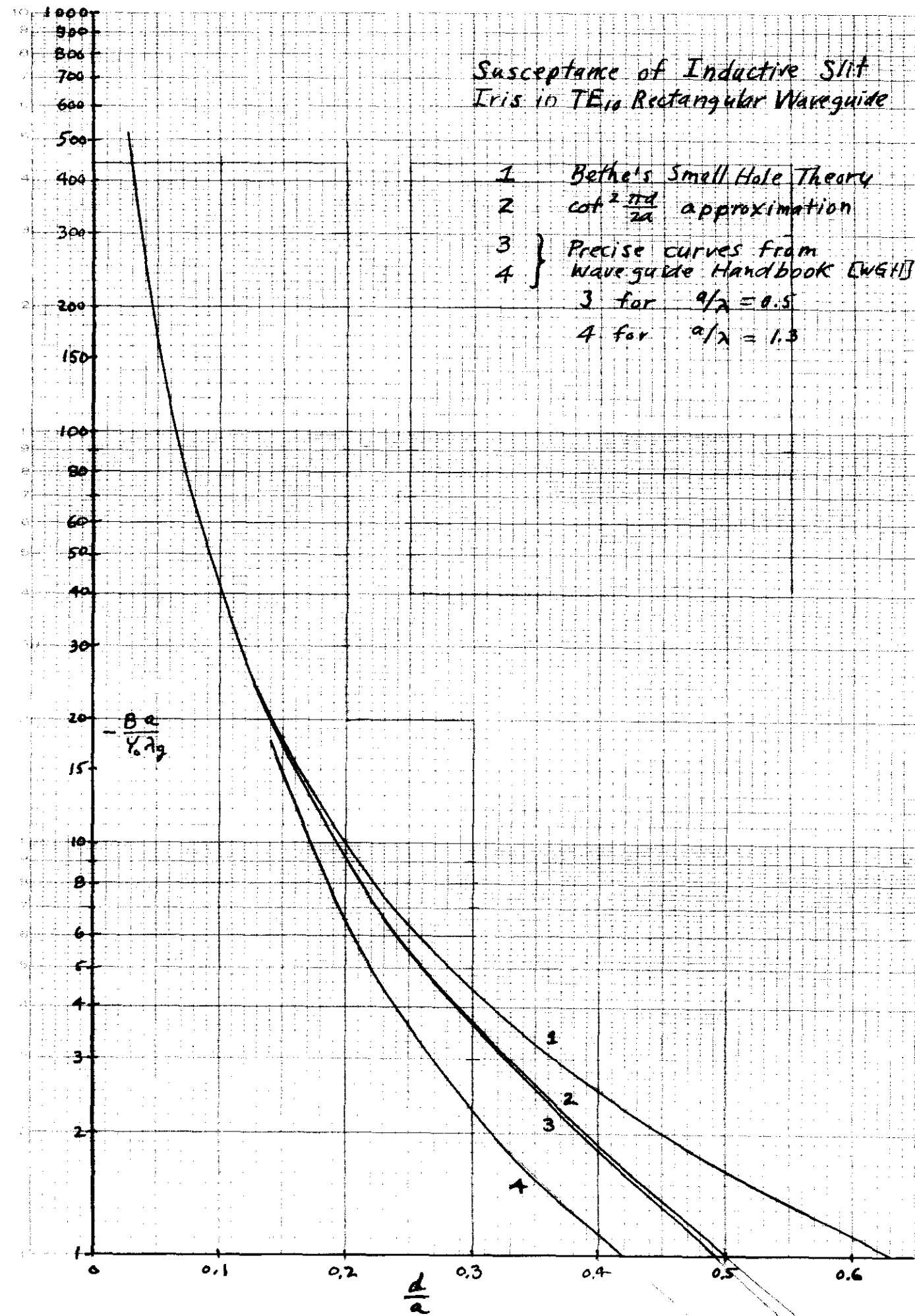
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Frequency Shift in TMO₂₀ Cylindrical Resonator Due To Inductive Slit Iris.

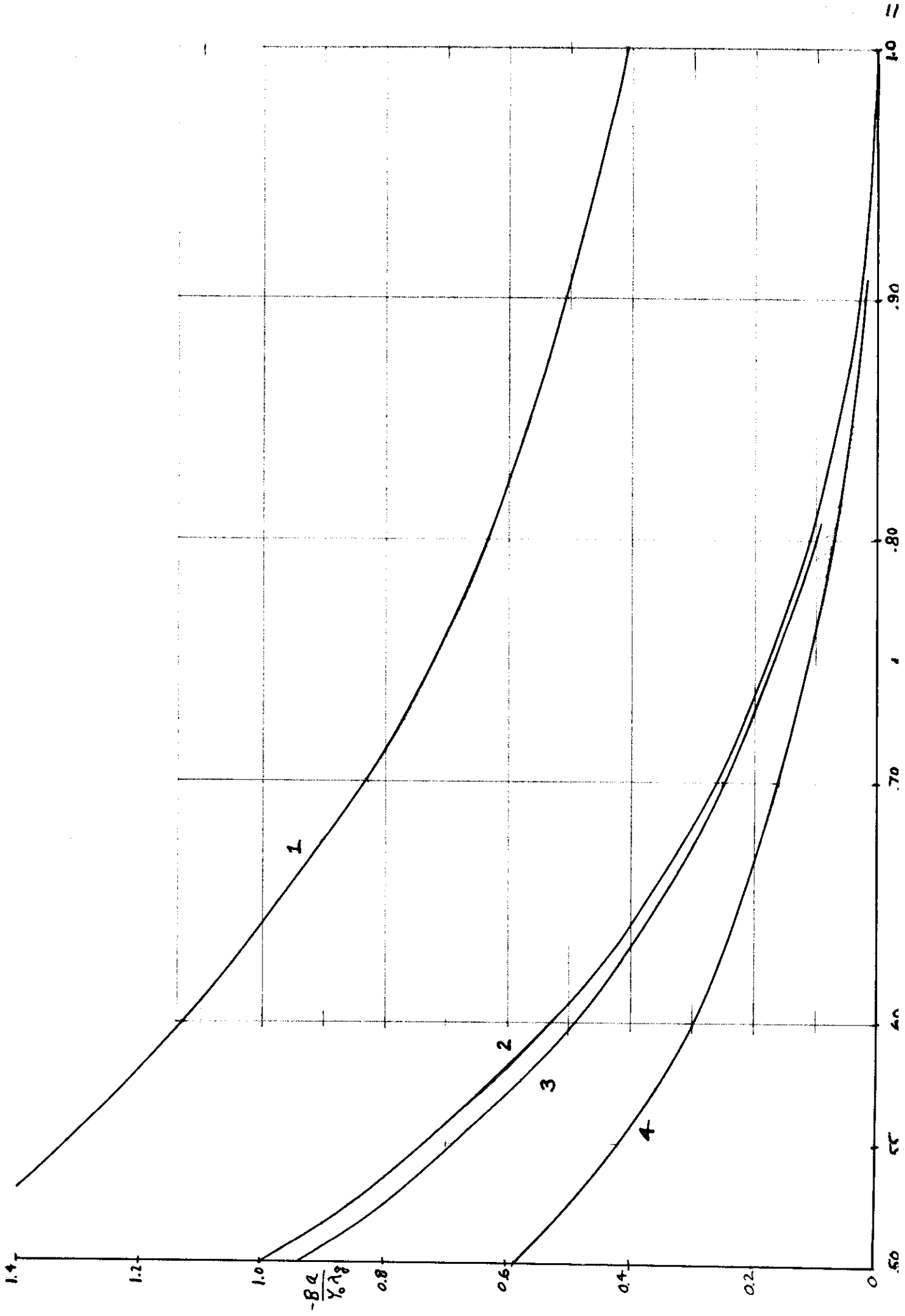


Experimental Points
o Direct
+ Indirect

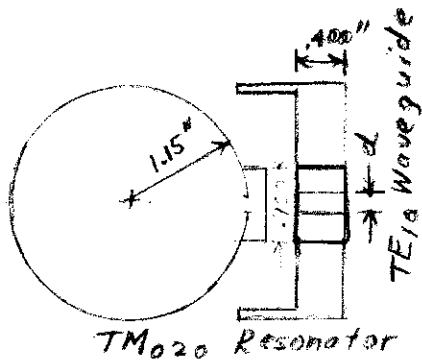
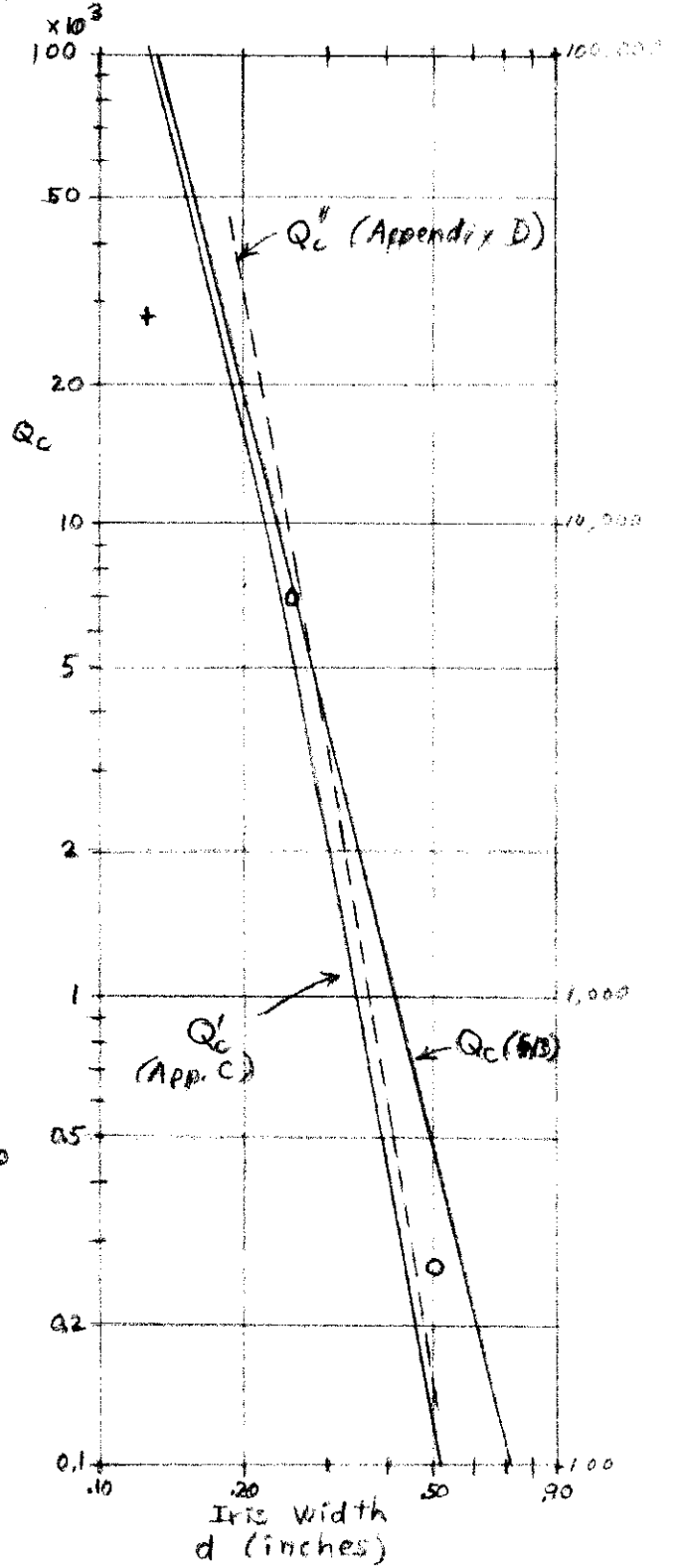
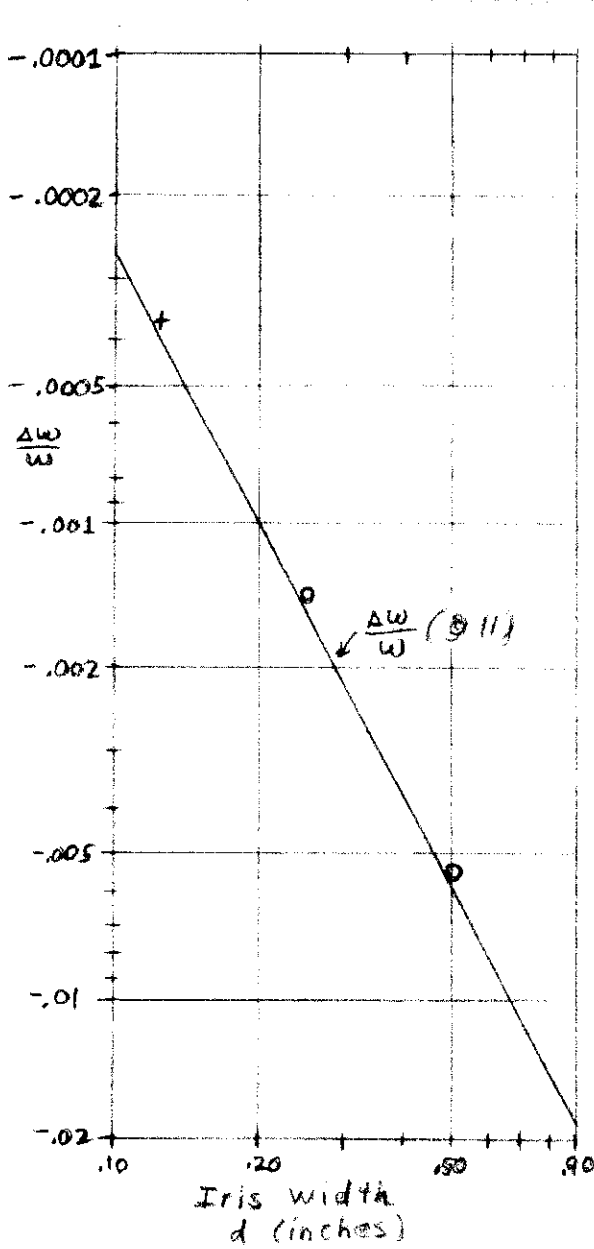
Susceptance of Inductive Slit Iris in TE₁₀ Rectangular Waveguide

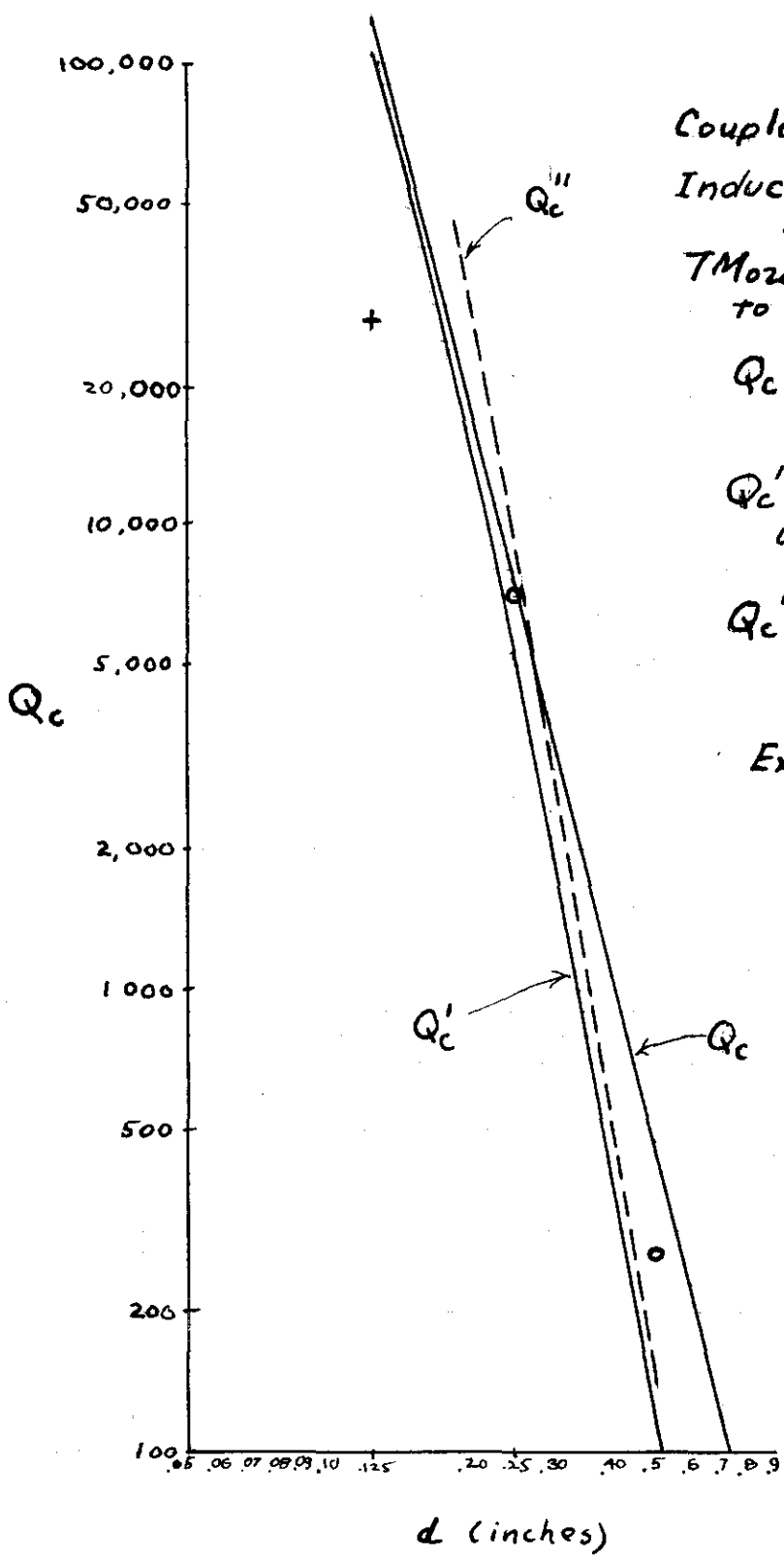


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Comparison of Approximate Theoretical Results with measured
 & Direct





Coupled Q_c
 Inductive Slit in \rightarrow d
 \rightarrow H
 TM₀₂₀ Circular Resonator to TE₁₀ Waveguide.
 Q_c from Bethe's Lumped Constant: $M_L = \frac{\mu L d^2}{16}$
 Q_c' from second approx. using $M_L = \frac{\mu L a^2}{4\pi} \tan^2 \frac{\pi a}{2a}$
 Q_c'' is Q_c' modified for finite wall thickness of .025".
 Experimental data .025" wall
 o Direct measurement
 + Indirect measurement